

Dynegy Midwest Generation, LLC 1500 Eastport Plaza Drive Collinsville, IL 62234

September 17, 2024 Illinois Environmental Protection Agency DWPC – Permits MC#15 Attn: 35 I.A.C. § 845.650(e) Alternative Source Demonstration Submittal 1021 North Grand Avenue East P.O. Box 19276 Springfield, IL 62794-9276

Re: Baldwin Power Plant Bottom Ash Pond; IEPA ID # W1578510001-06

Dear Mr. LeCrone:

In accordance with Title 35 of the Illinois Administrative Code (35 I.A.C.) Section (§) 845.650(e), Dynegy Midwest Generation, LLC (DMG) is submitting this Alternative Source Demonstration (ASD) for exceedances observed from the Quarter 2 2024 sampling event at the Baldwin Power Plant Bottom Ash Pond, identified by Illinois Environmental Protection Agency (IEPA) ID No. W1578510001-06.

This ASD is being submitted within 60 days from the date of determination of an exceedance of a groundwater protection standard (GWPS) for constituents listed in 35 I.A.C. § 845.600. As required by 35 I.A.C. § 845.650 (e)(1), the ASD was placed on the facility's website within 24 hours of submittal to the agency.

One hard copy is provided with this submittal.

Sincerely,

Phil Morris, PE Senior Director, Environmental

Enclosures

Alternate Source Demonstration, Quarter 2 2024, Bottom Ash Pond Baldwin Power Plant, Baldwin Illinois



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ALTERNATIVE SOURCE DEMONSTRATION

Baldwin Power Plant Bottom Ash Pond (Unit ID #601) IEPA ID: W1578510001-06 35 IAC 845.650

Prepared for

Dynegy Midwest Generation, LLC 1500 Eastport Plaza Drive Collinsville, Ilinois 62234

Prepared by

Geosyntec Consultants, Inc. 500 W. Wilson Bridge Road, Suite 250 Worthington, Ohio 43085

Project Number: GLP8068

September 12, 2024



Alternative Source Demonstration

Baldwin Power Plant Bottom Ash Pond (Unit ID #601) IEPA ID: W1578510001-06 35 IAC 845.650

Prepared for

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September 12, 2024

BPP BAP ASD

John Seymour, P.E. Senior Principal License No.: 062 040560 Expires: 11(3) OPS SE



August 2024



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ACRONYMS AND ABBREVIATIONS

%	percent
%0	per mille
ASD	alternative source demonstration
BAP	Bottom Ash Pond
bgs	below ground surface
BPP	Baldwin Power Plant
CCR	coal combustion residuals
cm/s	centimeters per second
DMG	Dynegy Midwest Generation, LLC
FAPS	Fly Ash Pond System
GWPS	groundwater protection standard
IAC	Illinois Administrative Code
IEPA	Illinois Environmental Protection Agency
LOE	line of evidence
mg/L	milligrams per liter
mg/kg	milligrams per kilogram
NAVD88	North American Vertical Datum of 1988
NMDS	nonmetric multidimensional scaling
NPDES	National Pollutant Discharge Elimination System
NRT	Natural Resource Technology, Inc.
PC	principal component
PCA	principal component analysis
SEP	sequential extraction procedure
XRD	X-ray diffraction

EXECUTIVE SUMMARY

Groundwater samples were collected at the Baldwin Power Plant (BPP) Bottom Ash Pond (BAP) during April 2024 for the Quarter 2, 2024 compliance monitoring event (Event 5 [E005]). They were evaluated for statistically significant exceedances of the groundwater protection standards (GWPS) as described in Title 35 of the Illinois Administrative Code (35 I.A.C.) § 845.600. Exceedances were identified for the following constituents and wells in the Uppermost Aquifer (UA):

- Chloride and lithium at well MW-370
- Fluoride at well MW-392
- Fluoride at well MW-393

These results are similar to GWPS exceedances determined during previous quarterly monitoring events, with the exception of the fluoride exceedance at well MW-392, which was a new exceedance determined after the E005 monitoring event. An Alternative Source Demonstration (ASD) was submitted in accordance with 35 I.A.C. § 845.660, and subsequently approved, for chloride exceedance at MW-370 and fluoride exceedance at MW-393 following the Second Quarter 2023 sampling event. An ASD was also submitted in accordance with 35 I.A.C. § 845.660, and subsequently approved, for a lithium exceedance at MW-370 following the First Quarter 2024 sampling event.

This ASD has been prepared to only provide information pursuant to 35 I.A.C. § 845.650(e) for the BAL BAP as a result of the newly identified E005 fluoride exceedance at MW-392.

There are four lines of evidence (LOEs) that demonstrate the BPP BAP (and the Fly Ash Pond, the other regulated CCR unit at the BPP) are not the source of the fluoride GWPS exceedance in well MW-392 and did not contribute to the exceedance. These four lines of evidence are:

- 1. If the BAP were the source of fluoride in groundwater, BAP porewater concentrations are expected to be greater than the concentrations in the UA. However, fluoride concentrations in the BAP porewater are historically more than 10 times lower than the minimum fluoride concentrations detected at MW-392.
- 2. Compliance monitoring location MW-392 has a similar geochemical signature as upgradient monitoring well MW-358. Moreover, a statistical evaluation (via PCA) has shown that their groundwater compositions are distinct from the porewater geochemical signature.
- 3. The stable boron and lithium isotopic ratios in groundwater at MW-370, which is screened within similar bedrock interval and lithology as compliance well MW-392, are similar to the ratio in groundwater at upgradient monitoring well MW-358. The similarity of the geochemistry in upgradient and downgradient groundwater provides further evidence that the likely source is the natural geology.



4. Solid phase analysis of rock cores from the uppermost aquifer (i.e., bedrock) identified fluoride within the naturally occurring minerals of the shale bedrock, thereby providing an alternative source of fluoride in groundwater. Based on a review of literature, elevated concentrations of fluoride are known to occur in groundwater within the shale-limestone bedrock (i.e., uppermost aquifer at the BAP) and is likely due to the influence of the solid phase composition.

Therefore, the fluoride exceedance is due to geochemical conditions within the UA which result in the mobilization of naturally occurring fluoride from site solids. This information serves as the written ASD prepared in accordance with 35 I.A.C. § 845.650(e), demonstrating that the BAP did not contribute to the fluoride exceedance observed at well MW-392 during the Quarter 2, 2024 sampling event (E005), rather, it is attributable to mobilization of naturally occurring fluoride. Therefore, assessment of corrective measures is not required for this fluoride exceedance at the BAP.



1. INTRODUCTION

Geosyntec Consultants, Inc. has prepared this alternative source demonstration (ASD) on behalf of Dynegy Midwest Generation, LLC (DMG), regarding the Bottom Ash Pond coal combustion residuals (CCR) unit at the Baldwin Power Plant (BPP) near Baldwin, Illinois. The ASD is completed pursuant to Title 35 of the Illinois Administrative Code (35 I.A.C.) Part 845 ("Standards for the Disposal of CCR in Surface Impoundments") and was completed by September 17, 2024, within 60 days of determination of the exceedances (July 19, 2024), as required by 35 I.A.C. Section 845.650(e). This report applies specifically to the CCR Unit referred to as the Bottom Ash Pond (BAP), identification (ID) number (No.) 601, IEPA ID No. W1578510001-06, and National Inventory of Dams ID No. IL50721.

A statistical exceedance of fluoride above the site-specific groundwater protection standard (GWPS) of 4.0 milligrams per liter (mg/L) was determined at downgradient monitoring well MW-392 following the Second Quarter 2024 sampling event (Ramboll 2024a). Statistical exceedances of chloride at downgradient monitoring well MW-370 and fluoride at downgradient monitoring well MW-393 were also determined following the Second Quarter 2023 sampling event (Ramboll 2023a). An ASD previously submitted to address these chloride and fluoride statistical exceedances for Second Quarter 2023 (Geosyntec 2023) was accepted by the Illinois Environmental Protection Agency (IEPA) on November 28, 2023 (IEPA 2023). Additionally, a statistical exceedance of lithium at downgradient monitoring well MW-370 was also determined following the First Quarter 2024 sampling event (Ramboll 2024b). An ASD was also submitted for the lithium exceedance at MW-370 (Geosyntec 2024) which was accepted by IEPA on August 8, 2024 (IEPA 2024). Therefore, these exceedances are not addressed in this ASD.

Under 35 I.A.C. Section 845.650(e), the owner or operator of a CCR surface impoundment may submit a demonstration that a source other than the CCR surface impoundment caused the contamination and the CCR surface impoundment did not contribute to the contamination, or that the exceedance of the groundwater protection standard resulted from error in sampling, analysis, statistical evaluation, natural variation in groundwater quality, or a change in the potentiometric surface and groundwater flow direction.

Pursuant to 35 I.A.C. Section 845.650(e), the lines of evidence (LOEs) documented in this ASD demonstrate that the BPP BAP CCR unit did not contribute to the GWPS exceedance for fluoride at downgradient monitoring well MW-392. Natural variability associated with the lithology of the aquifer is identified as the alternative source for the elevated fluoride concentrations at MW-392.

2. BACKGROUND

2.1 Site Location and Description

The BPP is in Randolph County and St. Clair County in southwest Illinois approximately 0.5 miles west-northwest of the village of Baldwin. The BPP property is bordered by Baldwin Road to the east; the village of Baldwin to the southeast; Illinois Central Gulf railroad tracks, State Road 154, and scattered residences to the south; the Kaskaskia River to the west; and farmland to the north. CCR impoundments present at the BPP include the BAP and the closed Fly Ash Pond System (FAPS), which included the West Fly Ash Pond, East Fly Ash Pond, and Old East Fly Ash Pond.

Non-CCR impoundments present at the BPP include the Secondary Pond, Tertiary Pond, and Baldwin Lake (BPP Cooling Pond). The locations of the CCR and non-CCR impoundments are shown in **Attachment 1**. The BAP is immediately north of the FAPS, which is a closed in-place CCR unit approved for closure by the IEPA on August 16, 2016.

2.2 Description of the CCR Unit

The BPP began operation in 1970 and initially burned bituminous coal from Illinois before switching to subbituminous coal in 1999. The BAP is an unlined surface impoundment with a surface area of approximately 177 acres used to store and dispose of sluiced bottom ash from the BPP, some of which is mined for beneficial reuse. The BAP is also used to temporarily store spray dry adsorption waste and to clarify plant process water, including other non-CCR station process wastewaters, which are then discharged in accordance with the station's National Pollutant Discharge Elimination System (NPDES) permit (AECOM 2016; IEPA 2016). The original construction date of the BAP is unknown but occurred sometime before 1981 based on a review of historical aerial photographs. Therefore, the unit is over 43 years old.

2.3 Geology and Hydrogeology

This section provides a summary of the site geology and hydrogeology; additional detail is provided in the Supplemental Hydrogeologic Site Characterization and Groundwater Monitoring Plan (Natural Resource Technology, Inc. [NRT] 2016) and the Hydrogeologic Site Characterization Report (Ramboll 2021).

Three hydrostratigraphic units are present at the BPP, which include the CCR, an unconsolidated Upper Unit, and a Bedrock Unit.

- CCR: Consists primarily of bottom ash, fly ash, and boiler slag and includes fill materials comprising predominantly of clays and silts excavated on-site for use in berm and road construction around the impoundment. Up to 28.2 feet of bottom ash has been observed towards the center of the BAP.
- Upper Unit (unconsolidated unit): Predominantly clay with silt and minor sand, silt layers, and occasional sand lenses, and includes lithologies identified as the Cahokia Formation, Peoria Loess, Equality Formation, and Vandalia Till. Thin sand seams present at the



contact between the Upper Unit and Bedrock Unit have been identified as potential migration pathways due to higher hydraulic conductivities in comparison to those in the surrounding clays (e.g., $\sim 10^{-4}$ centimeters per second [cm/s] in sands compared with $\sim 10^{-5}$ cm/s in clays) (Ramboll 2023b). Continuous sand seams have not been observed in the Upper Unit or immediately adjacent to the BAP. Due to the predominance of clay and only thin and intermittent sand lenses, this unit is not considered a continuous aquifer unit within the site boundary (NRT, 2016; Ramboll, 2021).

• Bedrock Unit: Pennsylvanian and Mississippian-aged interbedded shale and limestone continuously underlies the BPP and is considered the uppermost aquifer at the site. The top of bedrock ranges from 12.5 feet below ground surface (bgs) near the Kaskaskia River to 70 feet bgs within the East Fly Ash Pond (part of the FAPS). The Bedrock Unit is the uppermost aquifer, and ranges in thickness between 20 to 70 feet in thickness beneath the Site (Ramboll 2021).

A geologic cross-section originally included in the Hydrogeologic Site Characterization Report and locator map are provided as **Attachment 2**.

Groundwater at the site has previously been classified as Class II groundwater in accordance with 35 I.A.C. 620 based on the geometric mean hydraulic conductivity values measured in the monitoring wells screened in both the Upper Unit $(3.2 \times 10^{-5} \text{ cm/s})$ and the Bedrock Unit $(5.0 \times 10^{-6} \text{ cm/s})$ (NRT 2014).

The groundwater monitoring network for the BAP consists of 15 monitoring wells: 13 downgradient monitoring wells (MW-192, MW-193, MW-356, MW-369, MW-370, MW-382, MW-392, MW-393, MW-394, OW-256, OW-257, PZ-170, and PZ-182) and two background monitoring wells (MW-304 and MW-358) (**Attachment 1**). Monitoring wells are screened in both the uppermost aquifer (Bedrock Unit) from approximately 350 to 404 feet and the unconsolidated unit from 388 to 414 feet (North American Vertical Datum of 1988 [NAVD88]).

The potentiometric groundwater contours and generalized groundwater flow directions at the site are shown in **Attachment 3**. Groundwater flow in bedrock is toward the northwest in the eastern and central areas of the BAP, and southwest in the east area of the FAPS. Bedrock groundwater flows toward the Secondary and Tertiary Ponds, which were created in a former surface water drainage channel. Groundwater flow directions are generally consistent across sampling events. As shown in Attachment 3, MW-392 is upgradient of the FAPS. Therefore, the FAPS is not anticipated to influence the fluoride concentrations at MW-392.



3. ALTERNATIVE SOURCE DEMONSTRATION LINES OF EVIDENCE

This ASD for the fluoride GWPS exceedance at MW-392 is based on four LOEs. These LOEs are described and supported below.

3.1 LOE #1: BAP Porewater Concentrations of Fluoride are Lower than Groundwater Concentrations.

Porewater (*i.e.*, water within the CCR material of the BAP) samples have been collected from piezometer TPZ-164 since September 2018 and at five porewater wells (XPW-01, -02, -04, -05, and -06) since their installation in October 2022. Boring logs for TPZ-164 and XPW-01, -02, -04, -05, and -06 are provided in **Attachment 4**. CCR porewater is water "collected from the interstitial water between waste particles in surface impoundments as it occurs in the field" (USEPA 2014) and represents the material potentially leached from impoundments. The CCR materials are the primary source of constituent loading to the CCR porewater. Over an extended period (e.g., months to years), the CCR porewater reaches equilibrium with the CCR materials. The concentrations within the porewater are "the most representative data available for impoundments because these data are [field-collected] concentrations of leachate" (USEPA 2014). Porewater is therefore the most appropriate source term for potential flux out of CCR impoundments.

The fluoride concentrations reported for the porewater sampling locations are consistently less than the concentrations reported for fluoride at MW-392, as shown in **Figure 1**, making it improbable that the aqueous fluoride concentration would increase after it leached from the BAP. The highest detected fluoride concentration in the porewater is consistently more than 10 times lower than the maximum fluoride concentration reported at MW-392. The fluoride concentrations detected in the porewater samples are less than the lower confidence limits of fluoride concentrations reported at downgradient well MW-392 (4.07 mg/L calculated using a confidence band around a linear regression) (Ramboll 2024b), indicating that fluoride concentrations at MW-392 are not related to the BAP.

Given the generally conservative (non-reactive) nature of fluoride, its concentration is expected to remain stable or decrease along the flow path from the source due to dispersion and dilution. If the BAP were the source of fluoride in groundwater, BAP porewater concentrations would be expected to be greater than the concentrations in the groundwater.

3.2 LOE #2: MW-392 Has a Similar Ionic Composition to Upgradient Monitoring Well MW-358.

The groundwater at MW-392 has a similar ionic composition to the groundwater from background monitoring well MW-358, further indicating that MW-392 is not affected by the BAP. A Piper diagram, which is used for illustrating the relative concentration of major cations and anions in groundwater samples, shows that groundwater at MW-392 appears to be predominantly composed of chloride and monovalent cations, consistent with the composition of both background well

MW-358 and adjacent downgradient monitoring well MW-393, at which a previous fluoride exceedance was identified (**Figure 2**). This groundwater composition is different from the composition of samples of BAP porewater, which tends to have greater relative contributions of alkalinity, sulfate, and divalent cations such as calcium and magnesium (**Figure 2**).

Piper diagrams typically show the relative proportions and individual concentrations (respectively) of only major cations and anions. Advanced statistical approaches such as principal component analysis (PCA) or non-metric multidimensional scaling (NMDS) use a broader suite of analytes to evaluate the similarity or dissimilarity of different samples or groups and identify analytes that are main drivers for dissimilarities (Mumford et al., 2007).

PCA is often used to simplify large datasets with multiple variables by creating new uncorrelated variables known as principal components (PCs). The PCs are linear combinations of the original variables; the first few PCs typically capture most of the variation within the dataset. Factor loadings are calculated based on the correlation between PCs and the original variables. As such, variables with notably higher positive or negative factor loadings are main drivers of similarity or dissimilarity and clustering of samples. Factor scores are calculated based on the correlation between the combined chemical composition of each sample and the PCs. Samples with similar chemical compositions show similar factor scores and tend to cluster together on a PCA biplot.

In this ASD, the dataset used for PCA included 107 samples collected between 2022 and 2024 from background wells MW-304 and MW-358, downgradient wells MW-370, MW-392 and MW-393, and the BAP porewater wells.¹ The downgradient locations were selected based on observed statistical exceedances of the GWPS, the site hydrogeology and groundwater flow direction, and the spatial distribution of well locations. PCA requires that input variables have similar scales of measurement and variances. As such, data were standardized by mean-centering and scaling to unit variance prior to performing PCA. The fraction of total variation explained by each PC is shown in **Figure 3a**, with the first two PCs (Dimensions 1 and 2 on **Figure 3a**) accounting for approximately 69 percent (%) of the total variation in the datasets. Additionally, the quality of representation of each variable is presented in **Figure 3b**, demonstrating that for most variables, the majority of the variation is captured by the first two PCs.

PCA results are often visualized using biplots, where samples are projected on to the first two PCs (i.e., factor scores), and factor loadings are represented as vectors. The closer the data points are on the graph, the greater the similarity in their chemical composition. The biplot of PCA results from this study is shown on **Figure 4**, where the background samples are plotted in orange, the downgradient samples in dark blue, and the porewater samples in gray. The factor loadings, represented as vectors on the biplot, indicate that constituents such as calcium and barium are responsible for shifting the chemical signature of samples towards the porewater cluster. In contrast, constituents such as lithium, fluoride, and chloride are the main drivers for shifting chemical composition in the direction of the downgradient and background samples cluster. These

¹ Analytes included in this PCA include total alkalinity, boron, pH, barium, chloride, calcium, lithium, sulfate, and fluoride. The dataset used for PCA analysis is provided with this submission as **Attachment 5**.



results are generally consistent with the findings of the Piper diagram (**Figure 2**), which identified a higher relative abundance of chloride in the bedrock groundwater samples compared to CCR porewater.

Furthermore, as illustrated in the biplot (**Figure 4**), the porewater samples cluster separately from the downgradient and background wells. The biplot shows no overlap between the 95% bivariate confidence ellipses for: (i) porewater samples from within the BAP in gray, (ii) and downgradient and background bedrock groundwater samples in blue and orange (represented by the orange ellipse). These results are generally consistent with the findings of the Piper diagram (**Figure 2**), which identified clusters of porewater samples distinct from background and downgradient locations. Furthermore, the PCA demonstrates that background and downgradient samples cluster together, indicating that the chemical composition of the downgradient samples from MW-392 is relatively similar to background and other downgradient samples.

Clustering was further explored using Ward's hierarchical clustering method, a distance measure employed in agglomerative algorithms and commonly applied in hydrogeochemical studies. The analysis was performed on a scaled and centered dataset. As illustrated in the dendrogram (**Figure 5**), this analysis supported the distinction between porewater samples within the gray box and the combined group of downgradient and background groundwater wells in the orange box.

Non-metric multidimensional scaling (NMDS) analysis of the dataset from Q1 2023 to Q2 2024 was conducted to evaluate more recent site conditions and to further compare the combined chemical composition of porewater, background, and select downgradient samples. Additionally, the results of NMDS analysis can be used for validation of previous findings from PCA. As some wells were installed in 2022, the 2023 and 2024 samples are likely to be more representative of equilibrium conditions in the aquifer. While both PCA and NMDS aim to reduce dimensionality of multivariate datasets (e.g., the geochemical composition of waters) and visualize similarities among samples to interpret the underlying patterns, their methods are distinct. PCA relies on linear transformations and captures the maximum variance within datasets through orthogonal components, whereas NMDS utilizes non-metric rank orders to achieve a non-linear representation of the original distances between samples. Therefore, NMDS is more flexible in relation to input requirements, particularly as it does not require that datasets be normally distributed. NMDS analysis results are typically presented in two-dimensional space with arbitrary dimensions, where the distance between two samples is representative of their relative similarity.

The results of the NMDS on the BAL dataset are displayed in **Figure 6**. Qualitatively, the NMDS findings presented on **Figure 6** align closely with those from the PCA (**Figure 4**) and indicate that: (i) the porewater sample cluster (gray symbols) is separate from the downgradient (shades of blue) and background (shades of orange) samples; and (ii) the chemical compositions of the background and downgradient wells appear more similar to each other than to the composition of porewater. If BAP porewater was influencing the groundwater in downgradient wells MW-393 and MW-370, the groundwater geochemistry would be more similar to porewater. However, they are distinct and the similarity between upgradient and downgradient groundwater instead supports the conclusion that the groundwater composition is influenced by native lithology.



3.3 LOE #3: Stable Lithium and Boron Isotopes Provide Further Evidence that the UA has a Geochemical Signature Distinct from BAP Porewater.

Boron isotopes (¹¹B and ¹⁰B) can be useful tracers in groundwater systems in sedimentary environments (United States Geological Survey, 2004). Depleted (lower; or more negative) boron isotope ratios (reported as δ^{11} B, which is calculated as the ratio of ¹¹B/¹⁰B relative to an international standard) are an indicator of CCR constituents in aqueous samples due to the depleted δ^{11} B found in source coal (Ruhl et al. 2014) and coal ash. Alternatively, sediments formed during deposition from marine environments, such as the shales identified within the uppermost aquifer at the site, can be enriched in δ^{11} B (i.e., more positive values) during deposition (Spivack et al. 1987).

Aqueous samples were collected from select locations to represent multiple lithologies and locations relevant to the BAP, as summarized in **Table 1**. These locations included TPZ-164 to represent BAP CCR porewater conditions, and upgradient well MW-358 and compliance well MW-370 to represent wells screened within the downgradient shale (including compliance wells MW-392 and MW-393 screened within similar bedrock interval and lithology). MW-370 and MW-392 in the bedrock UA generally have a consistent geochemical signature, as indicated by the outcome of the PCA described in Section 3.2. The samples were submitted to SmartGas Sciences, LLC (Columbus, Ohio) for analysis of total boron and stable boron isotopes and to Isodetect GmbH (Leipzig, Germany) for analysis of total lithium and stable lithium isotopes.

If the BAP porewater were influencing the groundwater within UA, a similar isotopic distribution for boron and lithium between the porewater and groundwater would be expected. However, the boron stable isotopic signatures for the BAP CCR porewater and groundwater at MW-370 are markedly different, providing further evidence that the UA groundwater, which is similar in composition at both MW-370 and MW-392 based on the PCA analyses (summarized in Section , is dissimilar to the BAP. For the submitted samples, porewater from TPZ-164 had the most depleted δ^{11} B value, with a reported δ^{11} B of 2.8 per mille (‰).

The BAP porewater has a boron isotopic composition consistent with the reported δ^{11} B range for Illinois basin coal-derived CCR of -8.8‰ to 6.3‰ (Ruhl et al 2014) (**Figure 7**). Upgradient well MW-358 and compliance well MW-370 both had more positive δ^{11} B values, with reported results of 31.1‰ and 32.4‰, respectively (**Table 1**). The enrichment of δ^{11} B in these groundwater samples is inconsistent with influences from CCR. Instead, these results are consistent with elevated δ^{11} B values typically detected in shale formations, with these more positive values due to deposition in marine environments (Spivack et al., 1987; Warner et al., 2013). Typical ranges detected for δ^{11} B in groundwater unimpacted by CCR are 4.0‰ to 34.0‰ (Buszka et al., 2007; Warner et al., 2013). MW-258, an upgradient well screened within the interbedded limestone and shale formation had a δ^{11} B value (14.2‰) that was lower than what was detected at shale lithologies at MW-358 and MW-370, but still isotopically distinct from BAP porewater. This variability in δ^{11} B values within the bedrock at the Site may be attributed to differences in mineralogy or depositional environment over time.



Lithium isotopes (⁷Li and ⁶Li) are similarly useful tracers in groundwater and have been identified as particularly applicable for distinguishing water containing CCR constituents (Harkness et al., 2015). Lithium isotope ratios (reported as δ^7 Li, which is calculated as the ratio of ⁷Li/⁶Li relative to an international standard) can be an indicator of CCR constituents, as coals have δ^7 Li values ranging from -7.0 ‰ to 12.8‰, much lower than the ~31‰ commonly observed for seawater (Warner et al., 2014; Harkness et al., 2015). Release of ⁶Li from exchangeable sites on clays within shale during burial and formation can significantly alter groundwater δ^7 Li values compared to expectations based on the depositional environment (Warner et al., 2014).

MW-370 groundwater also has a lithium isotope composition ($\delta^7 \text{Li} = 20.7\%$) consistent with upgradient groundwater from shale lithologies at MW-358 ($\delta^7 \text{Li} = 26.0\%$), with slight differences potentially related to variations in burial history between the screening depths at these locations. The lithium data are provided in **Table 1** and presented on **Figure 8**, with the analytical laboratory report provided as **Attachment 6**. The lithium isotope signature for the BAP porewater ($\delta^7 \text{Li} = 17.1\%$) is somewhat similar to the bedrock lithium signature and is not consistent with the ranges of $\delta^7 \text{Li}$ for other CCR material effluents ($\delta^7 \text{Li}$ from -6.2 to 8.7‰; Harkness et al., 2015).

When examining the isotopic composition of MW-370 groundwaters using both boron and lithium isotope data in combination (**Figure 9**), it is clear that the BAP porewater is isotopically distinct for lithium and boron from all analyzed groundwaters. Together, these results provide further evidence that wells screened within the shale lithology, including at downgradient locations such as MW-392, is dissimilar to the BAP and instead are more strongly influenced by the bedrock lithology where they are screened. This is also consistent with results from both Piper diagram (**Figure 2**) and PCA analysis (**Figure 5**).

3.4 LOE #4: Fluoride Occurs Naturally in the Shale Bedrock of the Uppermost Aquifer.

Geosyntec reviewed the results of analyses completed on solid phase samples collected from the Site to support the conclusion that statistical exceedances of the site-specific fluoride GWPS at MW-392 are associated with the limestone and shale bedrock formation. Solid phase analysis identified fluoride within the bedrock of the uppermost aquifer at the Site – i.e., it is a naturally occurring inorganic substance within the mineral matrix of the bedrock (Attachment 7). The presence of fluoride within the solid phase of the uppermost aquifer (bedrock) likely contributes to elevated and naturally occurring fluoride in the groundwater.

Solid phase analysis of bedrock from compliance location MW-392 via X-ray diffraction (XRD) identified fluoride-bearing minerals in the solid phase materials (**Attachment 8**). The boring logs for MW-392 and MW-358 are provided in **Attachment 4**. Fluorapatite [Ca₅(PO₄)₃F], a fluoride-bearing mineral, was identified in samples collected from the shale formation at downgradient well MW-392 (**Table 2; Attachment 8**). The highest abundance of fluorapatite (2.7%) was identified in a sample collected at 80 to 82 feet below ground surface at downgradient well MW-392. This sample is at the same depth as the screened interval for MW-392. The presence of fluoride within



the aquifer solids of the shale in the uppermost aquifer, including the presence of a fluoride-bearing mineral, provide an alternative source for fluoride in groundwater other than the BAP.

Studies have found that fluoride concentrations in groundwater are comparable to or higher than those observed at MW-392 and are often found within the Pennsylvanian and Mississippian-aged interbedded shale and limestone of the uppermost aquifer. A USGS summary found that water within the upper parts of the Pennsylvanian-aged aquifers is generally similar throughout the Illinois and Indiana basins (Cable et al, 1971). This groundwater is influenced by the interaction with the variable interbedded rock types present in the uppermost aquifer at the BAP and can vary from a sodium bicarbonate to a sodium chloride type within a few feet of change in depth (Lloyd and Lyke 1995). Similarly, Lloyd and Lyke (1995) noted that "the fluoride content of the water [in Pennsylvanian-aged aquifers] is great enough to mottle the teeth of persons who drink it on a continual basis," with concentrations reported as high as 15 mg/L.

These results suggest that contact with Pennsylvanian-aged bedrock can result in natural variability in the reported fluoride concentrations in groundwater at ranges consistent with those detected at the site.

4. CONCLUSIONS

It has been demonstrated that the fluoride GWPS exceedance at MW-392 is not caused by a release from the BAP CCR unit, but instead is attributed to natural lithology at the site. The following summarizes the four LOEs used to support this demonstration:

- 1. If the BAP were the source of fluoride in groundwater, BAP porewater concentrations are expected to be greater than the concentrations in the UA. However, fluoride concentrations in the BAP porewater are historically more than 10 times lower than the minimum fluoride concentrations detected at MW-392.
- 2. Compliance monitoring location MW-392 has a similar geochemical signature as upgradient monitoring well MW-358. Moreover, a statistical evaluation (via PCA) has shown that their groundwater compositions are distinct from the porewater geochemical signature.
- 3. The stable boron and lithium isotopic ratios in groundwater at MW-370, which is screened within similar bedrock interval and lithology as compliance well MW-392, are similar to the ratio in groundwater at upgradient monitoring well MW-358. The similarity of the geochemistry in upgradient and downgradient groundwater provides further evidence that the likely source is the natural geology.
- 4. Solid phase analysis of rock cores from the uppermost aquifer (i.e., bedrock) identified fluoride within the naturally occurring minerals of the shale bedrock, thereby providing an alternative source of fluoride in groundwater. Based on a review of literature, elevated concentrations of fluoride are known to occur in groundwater within the shale-limestone bedrock (i.e., uppermost aquifer at the BAP) and are likely due to the influence of the solid phase composition.

The alternative source of fluoride is the shale bedrock lithology, whose geochemistry influences the groundwater composition. This demonstration meets the expectations in both 35 I.A.C. 845.650(e) and the technical manual for the Municipal Solid Waste Landfill federal regulatory program (Code of Federal Regulations, Title 40, Section 258) that a statistically significant increase may result from natural variation in groundwater quality and that the BAP is not the source of the increase in fluoride at MW-392 and does not contribute to the exceedance.

The information serves as the written ASD prepared in accordance with 35 IAC 845.650(e) demonstrating that the BAP CCR unit did not contribute to the GWPS exceedance for fluoride at MW-392. Therefore, implementation of corrective measures is not required for fluoride at the BAP CCR unit.

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TABLES

Sample ID	Sample Location	Sample Description	Total Boron (µg/L)	δ ¹¹ Β (‰)	+/- (2SE)	Total Lithium (µg/L)	δ ⁷ Li (‰)	+/- (2SE)
20230206 TPZ-164	TPZ-164	Porewater	1116	2.8	1.2	28	17.1	0.75
20230206 Cooling Pond	Cooling Pond	Surface Water	240	5.7	1.2	3.1	35.2	0.74
20230206 MW-370	MW-370	Downgradient Shale	2061	32.4	1.2	227	20.7	0.73
20230206 PZ-170	PZ-170	Downgradient PMP	326	43.2	1.2	44	17.1	0.73
20230206 MW-158R	MW-158R	Background PMP	86	18.0	1.2	23	31.5	0.54
20230207 MW-358	MW-358	Background Deep Shale	1778	31.1	1.2	185	26.0	0.7
20230207 MW-258	MW-258	Background Shale	1248	14.2	1.2			

Notes:

%: parts per thousand (per mille)

µg/L: micrograms per liter

--: Sample not analyzed

PMP: potential migration pathway

SE: standard error

Table 2 - Summary of Rietveld Quantitative Analysis X-Ray Diffraction Results Baldwin Power Plant

	MW-358	MW-358	MW-392	MW-392	MW-392		
	(47-49)	(86-88)	(32-33.5)	(66-68)	(80-82)		
	Upgradient	Upgradient	Downgradient	Downgradient	Downgradient		
	Shallow Shale	Deeper Shale Body	Clay with increasing sand content	Shale	Shale transitioning to limestone		
Mineral/Compound	Formula	Mineral Type	(wt %)	(wt %)	(wt %)	(wt %)	(wt %)
Quartz	SiO ₂	Silicate	29.2	30.7	53.5	22.7	29.8
Muscovite	KAl ₂ (AlSi ₃ O ₁₀)(OH) ₂	Mica	18.8	19.7	13.1	15.9	13.1
Albite	NaAlSi ₃ O ₈	Feldspar	0.4	2.5	8.5	0.6	0.6
Microcline	KAlSi ₃ O ₈	Feldspar	8.6	5.9	6.8	5.1	1.0
Diaspore	aAlO.OH	Oxyhydroxide	-	-	-	2.8	-
Magnetite	Fe ₃ O ₄	Oxide	0.5	0.3		0.1	1.4
Anatase	TiO ₂	Oxide	0.8	1.8	-	1.0	0.8
Calcite	CaCO ₃	Carbonate	0.5	1.0	-	14.9	28.1
Fluorapatite	Ca ₅ (PO ₄) ₃ F	Phosphate	-	-		0.2	2.7
Ankerite	CaFe(CO ₃) ₂	Carbonate	-	-		0.8	-
	·		Clay Minerals				
Kaolinite	$Al_2Si_2O_5(OH)_4$	Kaolin	4.8	15.0	7.5	3.6	5.5
Montmorillonite	$(Na,Ca)_{0.3}(Al,Mg)_2Si_4O_{10}(OH)_2 \bullet 10H_2O$	Smectite	6.8	4.8	0.0	5.8	3.5
Nontronite	Fe2(Al,Si)4O10(OH)2Na0.3(H2O)4	Smectite	4.6	4.3		3.3	4.2
Illite/Montmorillonite	$KAl_4(Si,Al)_8O_{10}(OH)_4 \bullet 4H_2O$	Mixed Layer I/S	8.8	2.7		7.1	3.6
Illite	K(Al,Mg,Fe) ₂ (Si,Al) ₄ O ₁₀ (OH) ₂	Illite	15.0	9.2		10.4	4.1
Chlorite	(Fe,(Mg,Mn)5,Al)(Si3Al)O10(OH)8	Chlorite	1.3	2	7.0	6.1	1.6
	Clay Minerals Total		41	38	15	36	23
	Clays + Muscovite Total	60	58	28	52	36	

Notes

Only samples collected within the shale bedrock are shown. Additional sample data is provided in Attachment 8.

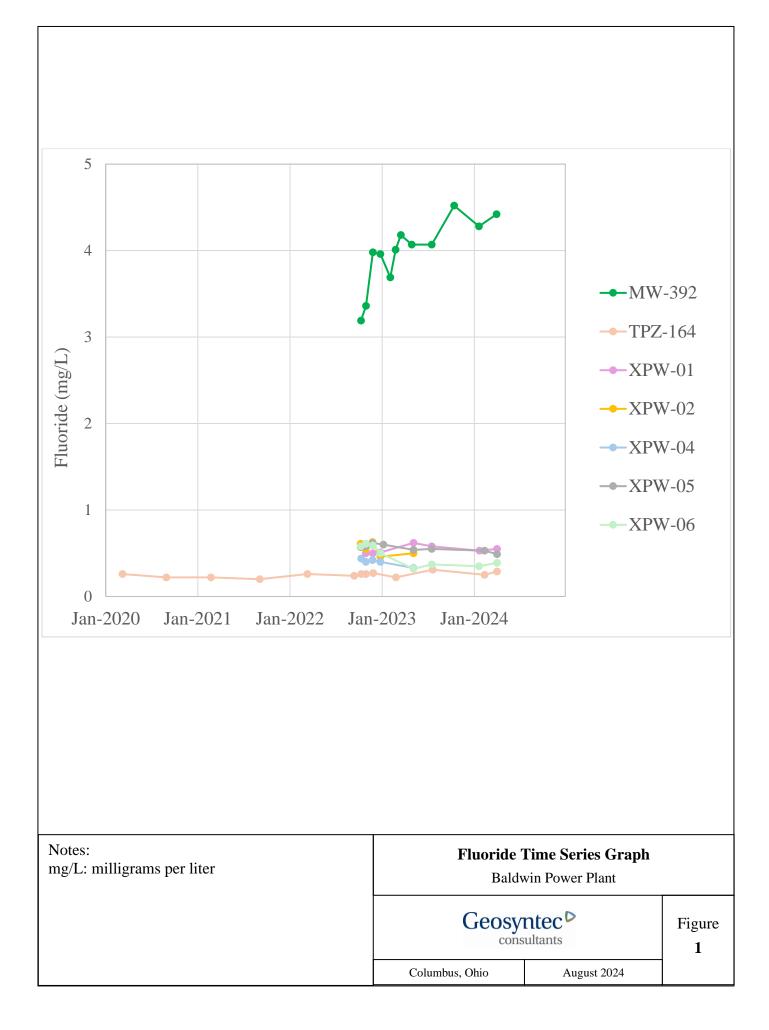
Dashes indicate that the mineral was not identified by the analyst and not included in the refinement calculation for the sample

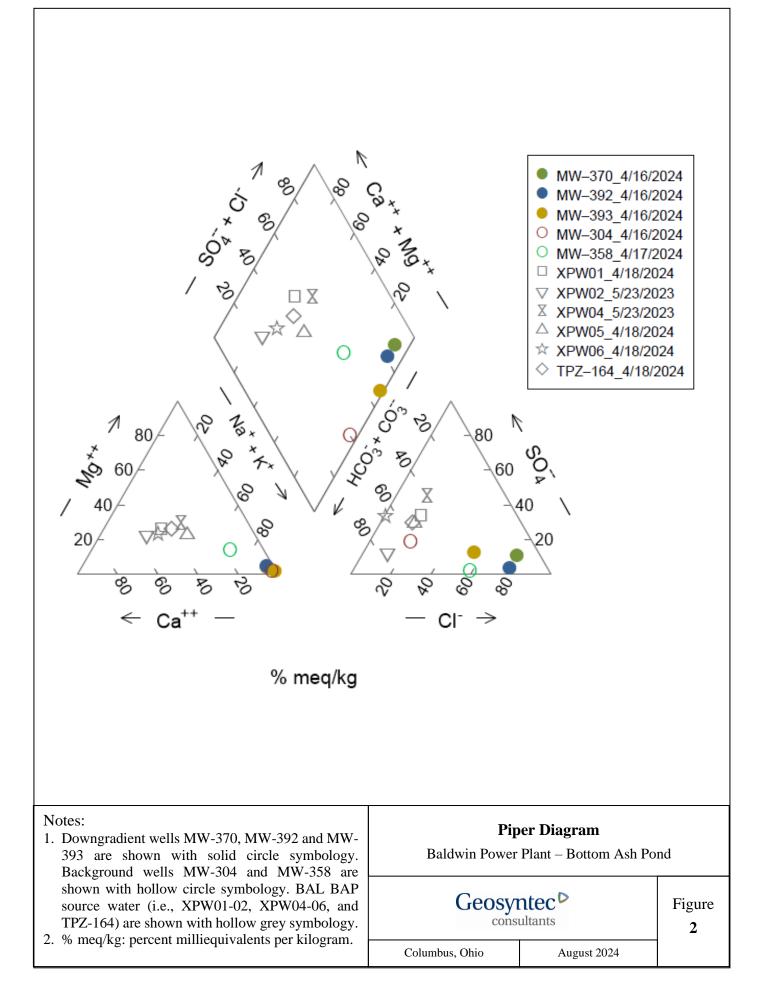
The weight percent quantities indicated have been normalized to a sum of 100%. The quantity of amorphous material has not been determined.

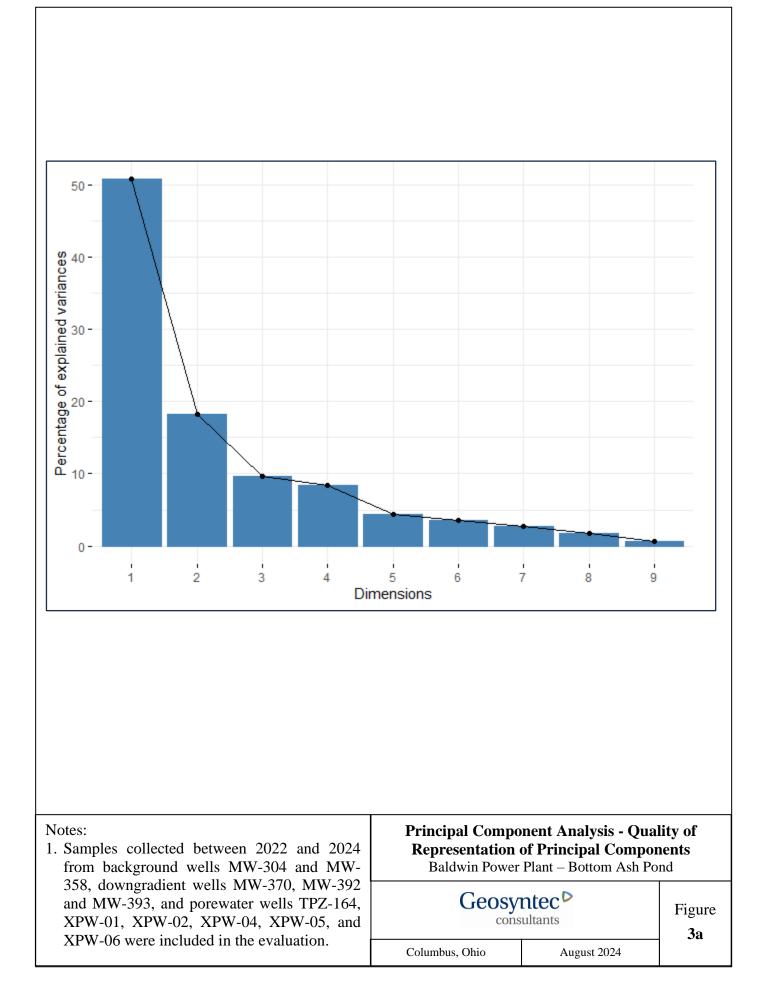
Sample depths are shown in feet below ground surface (ft bgs).

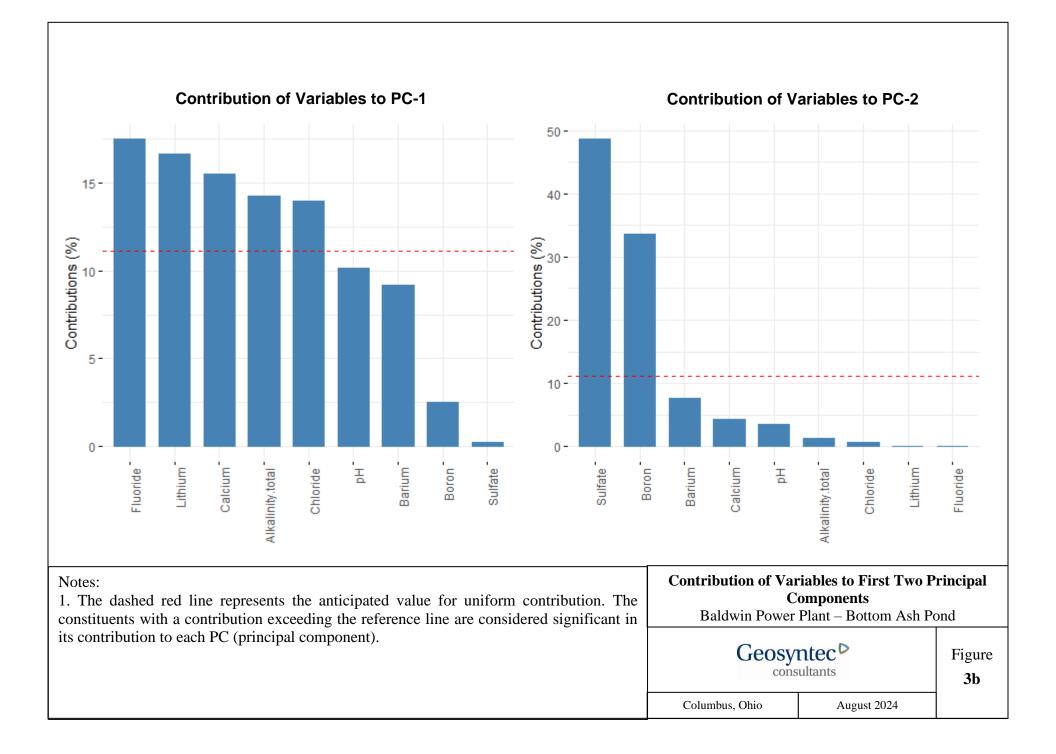
wt %: percentage by weight

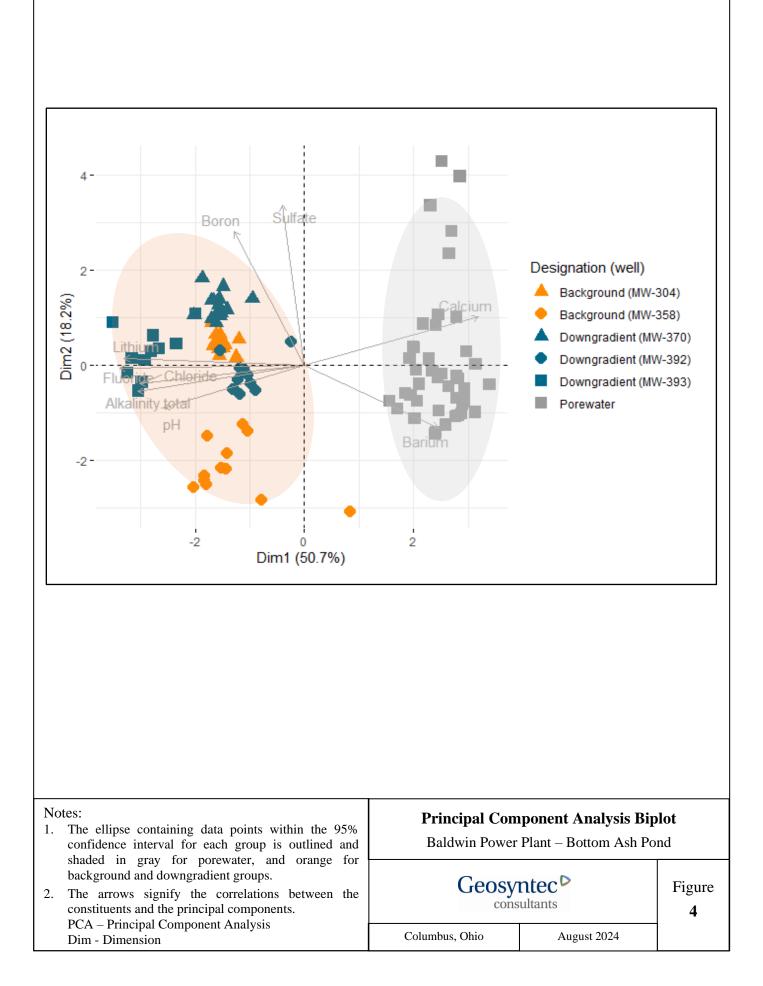
FIGURES

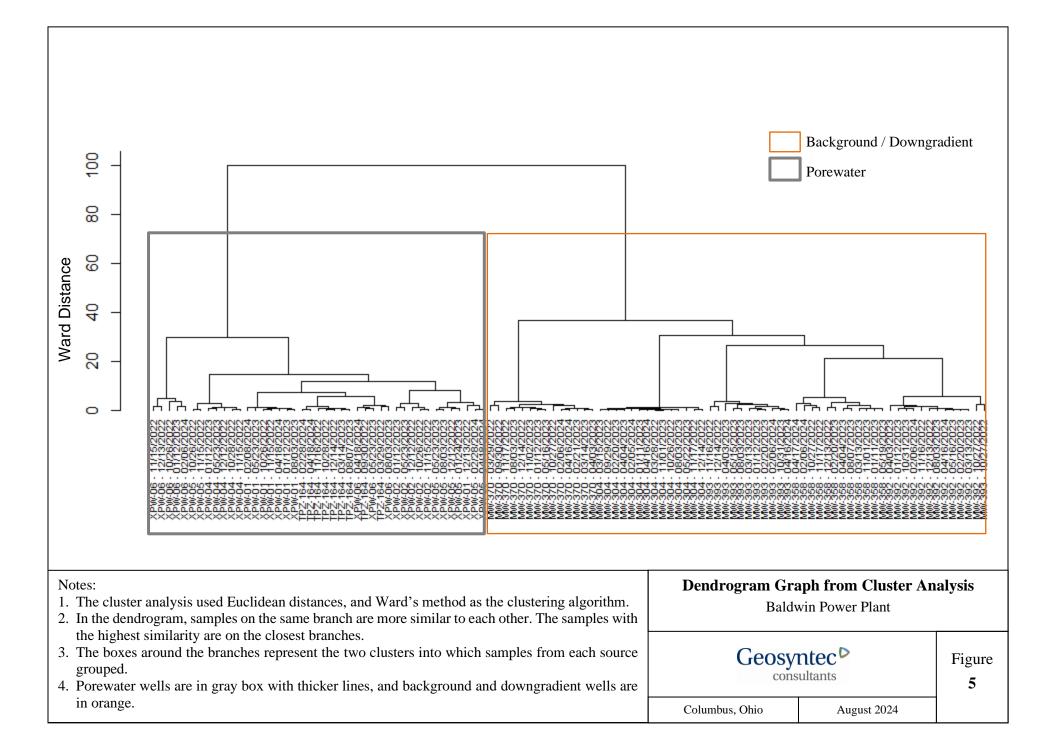


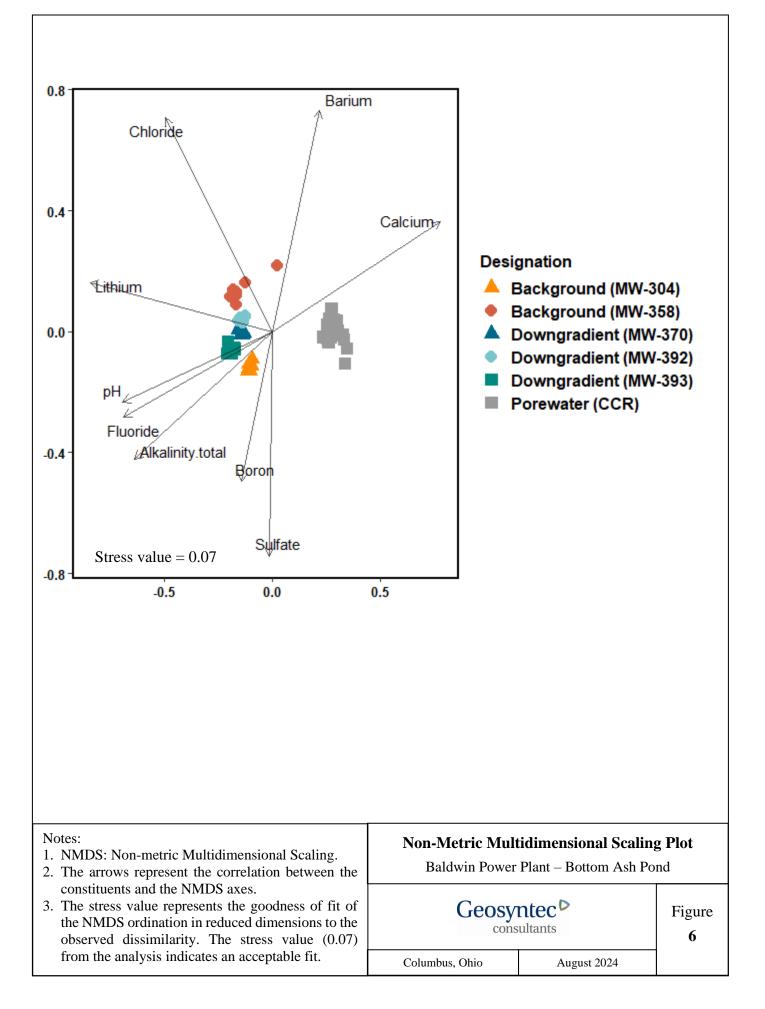


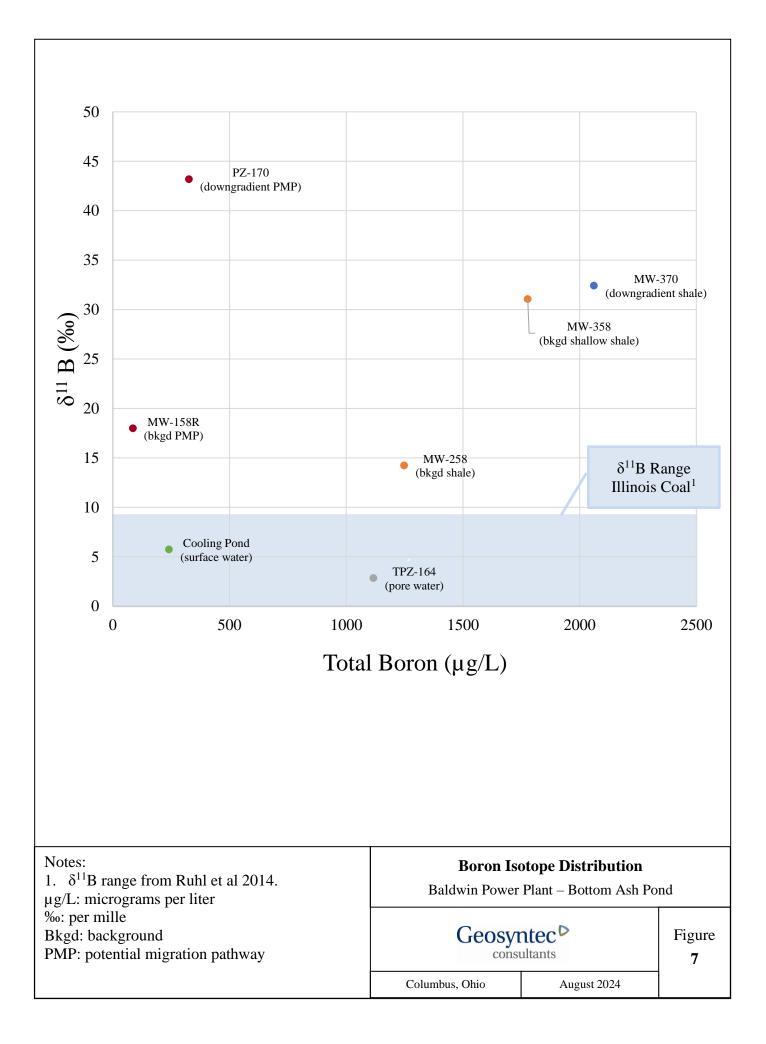


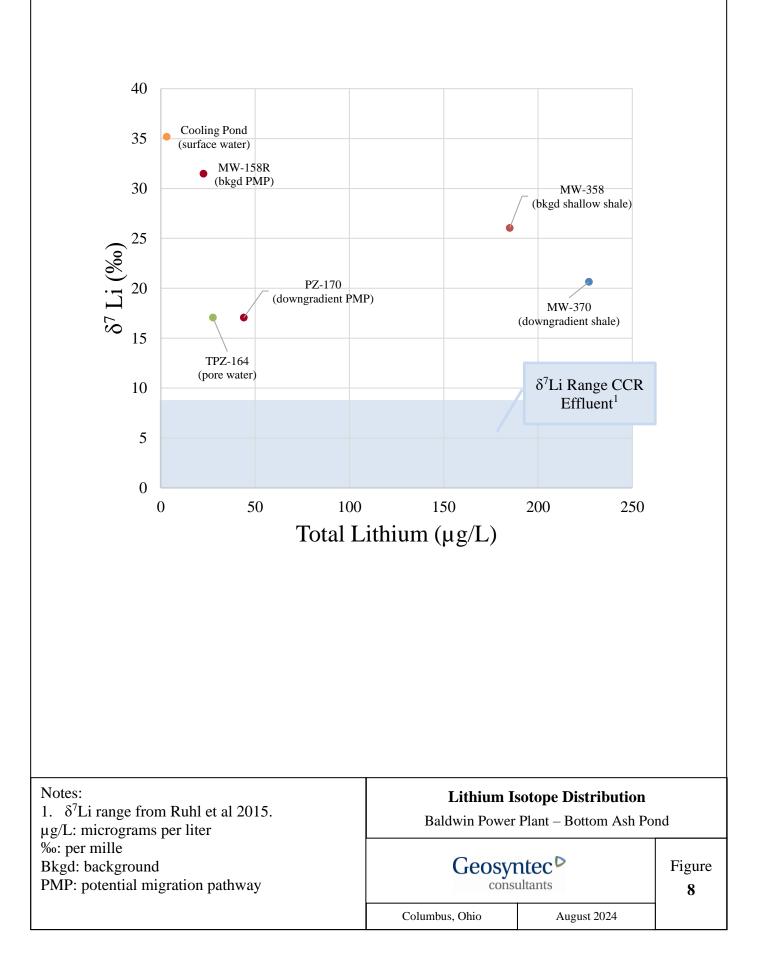


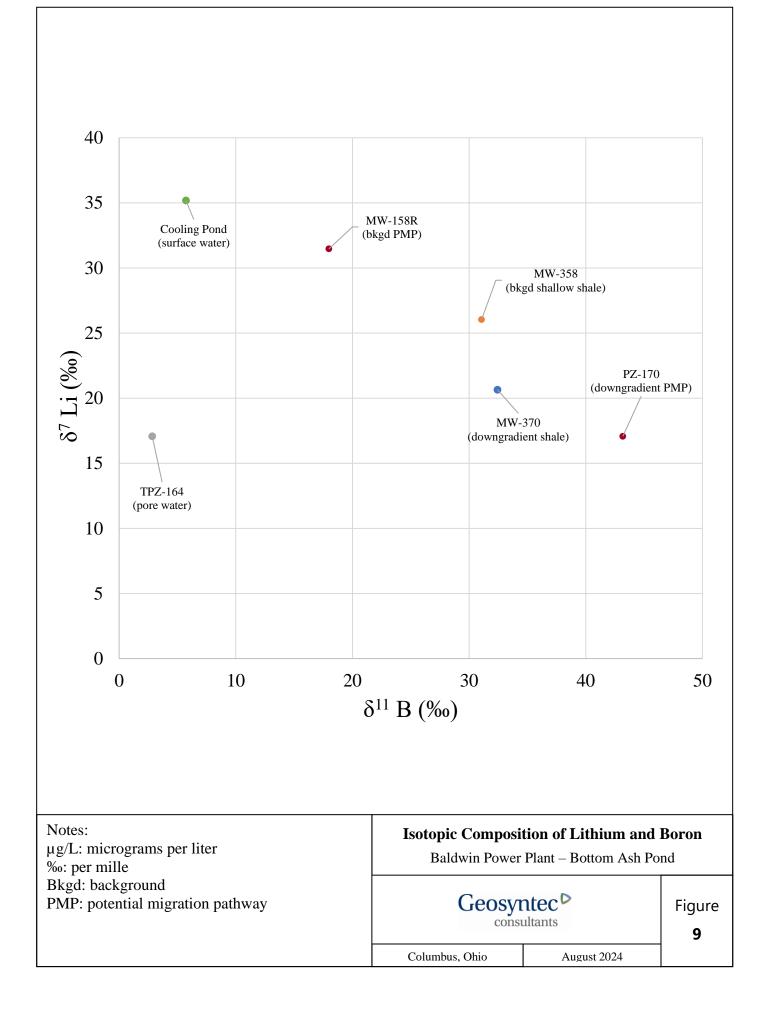




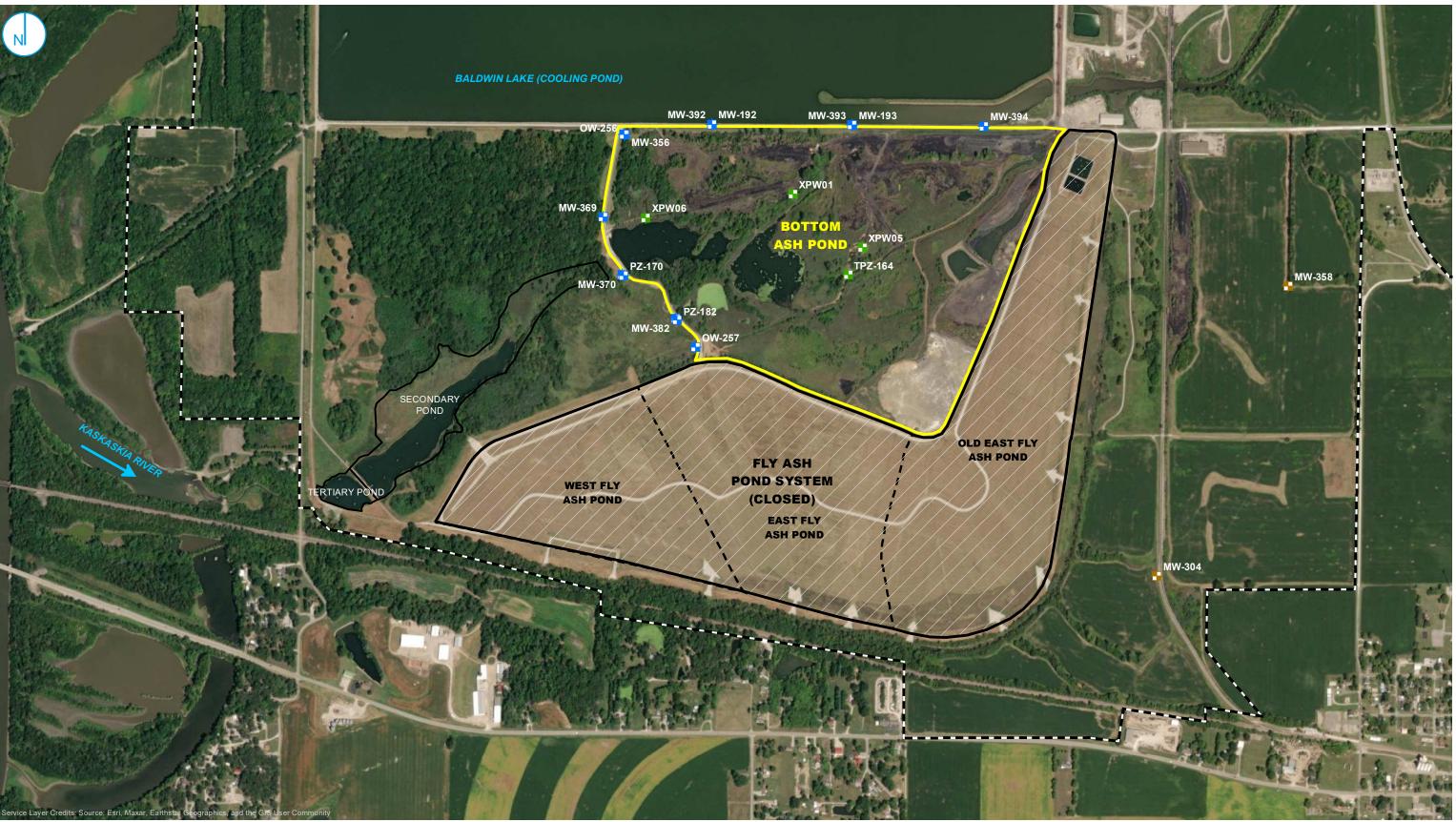








ATTACHMENT 1 Part 845 Groundwater Monitoring Network



BACKGROUND WELL COMPLIANCE WELL PORE WATER WELL

> 800 _ Feet

400

REGULATED UNIT (SUBJECT UNIT) SITE FEATURE CAPPED AREA PROPERTY BOUNDARY

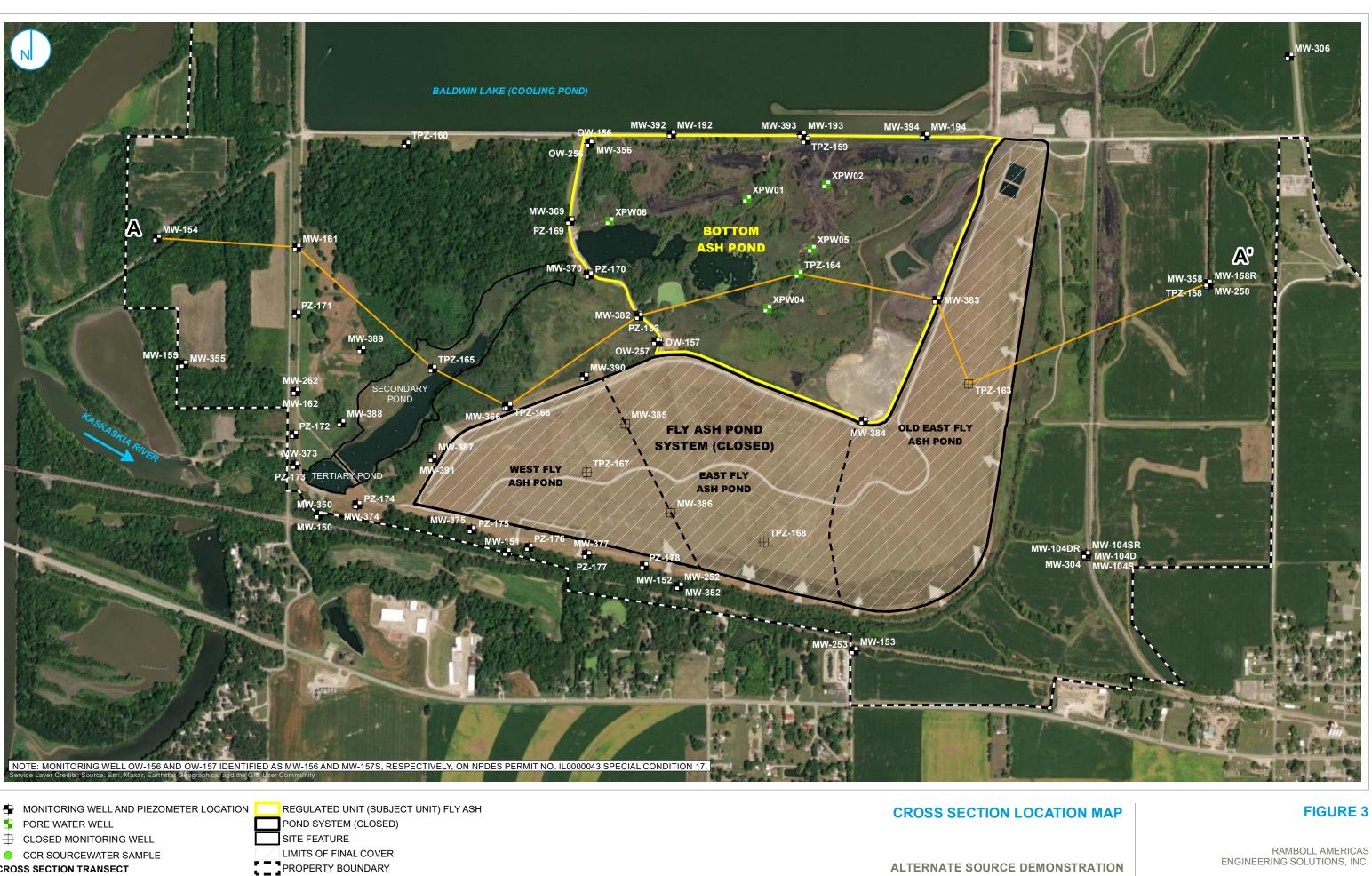
35 IAC § 845.600 GROUNDWATER MONITORING SYSTEM

BOTTOM ASH POND BALDWIN POWER PLANT BALDWIN, ILLINOIS

RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.



ATTACHMENT 2 Geologic Cross Section



CROSS SECTION TRANSECT

800

Foot

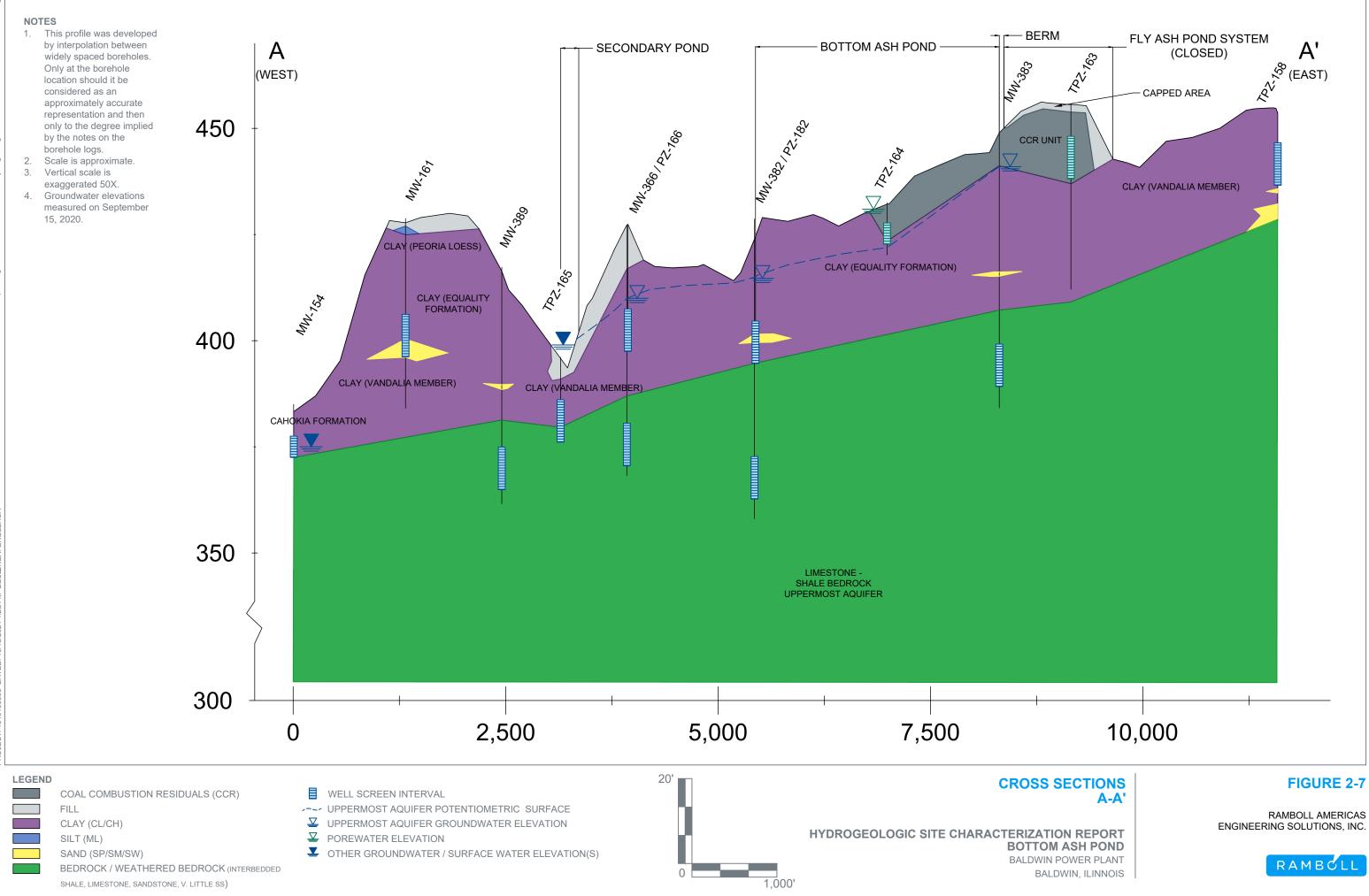
- A to A'

400

ALTERNATE SOURCE DEMONSTRATION BOTTOM ASH POND BALDWIN POWER PLANT BALDWIN, ILLINOIS

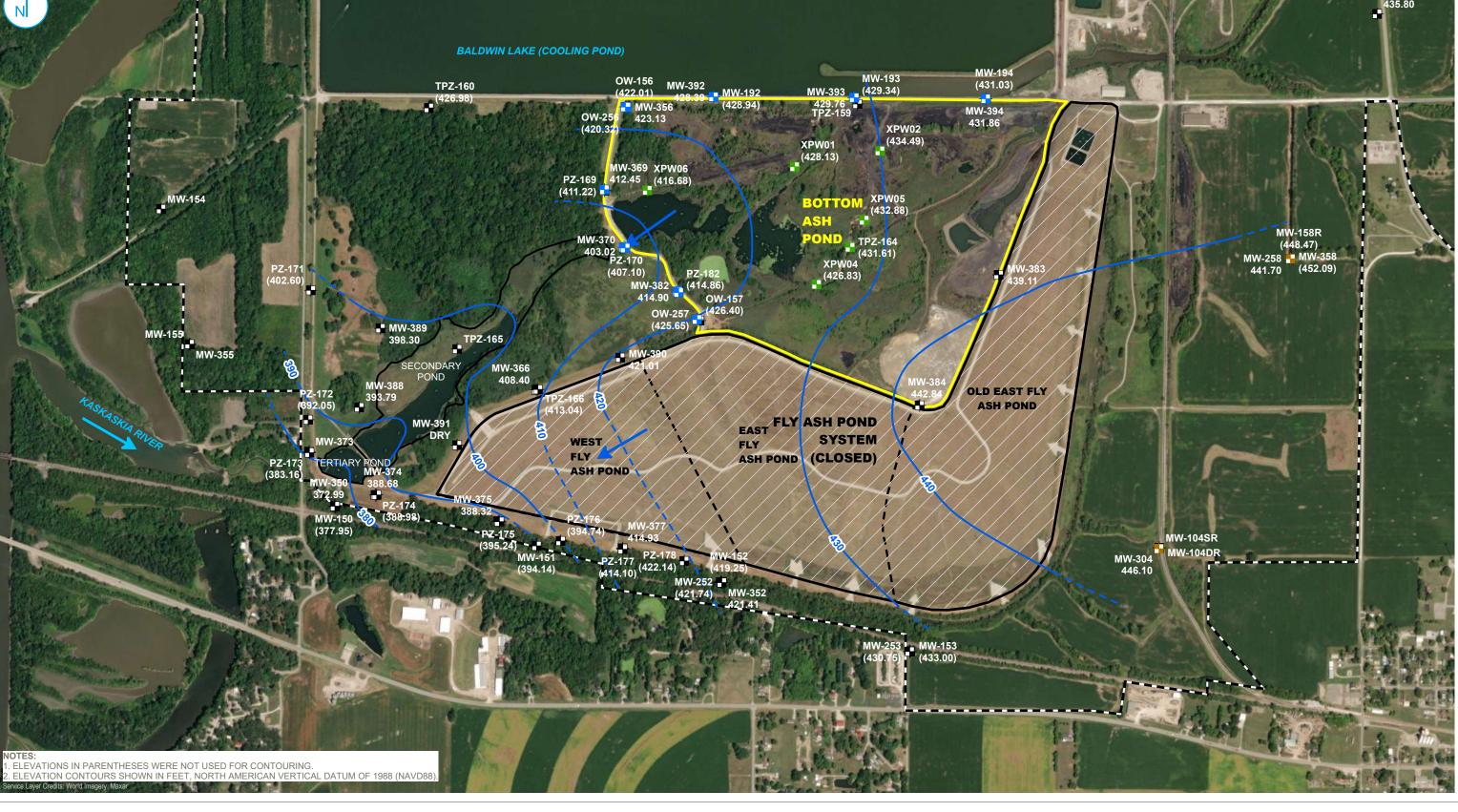
RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.





ATTACHMENT 3

Uppermost Aquifer Potentiometric Surface Map – April 15, 2024



- COMPLIANCE MONITORING WELL
- BACKGROUND MONITORING WELL
- MONITORING WELL
- PORE WATER WELL
- CONTOUR (10-FT CONTOUR INTERVAL, NAVD88)
 INFERRED GROUNDWATER ELEVATION CONTOUR
 - → GROUNDWATER FLOW DIRECTION

GROUNDWATER ELEVATION

FLY ASH POND SYSTEM (CLOSED)
 SITE FEATURE
 CAPPED AREA
 PROPERTY BOUNDARY

REGULATED UNIT (SUBJECT UNIT)

POTENTIOMETRIC SURFACE MAP APRIL 15, 2024

2024 ANNUAL GROUNDWATER MONITORING AND CORRECTIVE ACTION REPORT



BALDWIN POWER PLANT BALDWIN, ILLINOIS RAMBOLL AMERICAS ENGINEERING SOLUTIONS, INC.



ATTACHMENT 4 Boring Logs



Blake Weller Cascade Drilling 10/5/2022 10/8/2022 Sonic Common Well Name MW358 Final Static Water Level Feet (NAVD88) Surface Elevation 453.59 Feet (NAVD88) Borehole Diame 6.0 inc Local Grid Origin (estimated:) or Boring Location ⊠ State Plane S56,726.63 E E/30 Lat 38° 11' 42.9882" Local Grid Location 1/4 of 1/4 of Section T N. R Long -89° 50' 57.9018" Feet N Facility ID County Randolph State IL Baldwin State Baldwin Soil Properties Set Set Sample Soil/Rock Description And Geologic Origin For Each Major Unit Signer Sig	Facility/P						Lice	ense/P	Permit	/Moi	nitorin	g Nur	nber		Boring	g Num		of	5
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				Boring Number MW358								ge 2	of	5
Sar	nple							amp		Soil	Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic	Log Well	Diagram PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
					(CL/ML)		1							
2	60		-13	13 - 17.8' SILTY CLAY: CL/ML, grayish brown (10YR 5/2), strong brown (7.5YR 5/6) and very dark brown (10YR 2/2) mottling (20-30%), low toughness, medium to high plasticity, stiff to very stiff.	— — —									
2 CS	60		16	16.1' mottling discontinues.	CL/ML									
з СS	48 36		- 18 - 19 - 20 - 21	17.8 - 21' SILTY CLAY WITH SAND: (CL/ML)S, brown (10YR 5/3), strong brown (7.5YR 5/6) and gray (10YR 6/1) mottling (20-30%), gravel (5-15%), no dilatancy, high toughness, low to medium plasticity, hard, moist. 21 - 26.5' SHALE: BDX (SH), dark gray (GLEY 1 4/N), weathered, thin bedding, moderately fractured.	(CL/ML)									
4 CORE	36 32		-22 -23 -24 -25 -26	24' -25.2' wet.	BDX (SH)									RUN #4: Modified RQD = (21/32) = 66%
5 CORIE	36 29		-27	26.5 - 27.5' LIMESTONE: BDX (LS), dark gray (5Y 4/1), shaley, fossiliferous, very strong. 27.5 - 31.3' SHALE: BDX (SH), grayish black (N2), weathered, highly decomposed to residual soil, wet to moist.	BDX (LS)									RUN #5: Modified RQD = (0/29) = 0%
6 CORE	72 60		-29	29.3' thinly bedded, moderately decomposed. 30' slightly decomposed to competent, moderately fractured. 31.3 - 32' COAL: COAL, black (N1).	BDX (SH)									RUN #6: Modified RQD = (45/60) = 75%
			-32		COAL									



				Boring Number MW358							Pag		of	5
Sar	nple							duu		Soil	Prop	erties		_
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Loo	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
7 CORE			-33 -34 -35 -36 -37 -38 -39	32 - 33' SHALE: BDX (SH), grayish black (N2), slightly decomposed to competent, moderately fractured, wet to moist. 33 - 36' SHALEY LIMESTONE: BDX (LS/SH), medium gray (N5), weathered, shaley, higly decomposed, slightly fractured. 36 - 40.8' SHALEY LIMESTONE: to SHALE: BDX (LS/SH), interbedded shale.	BDX (SH) BDX (LS/SH									RUN #7: Modified RQD = (67/71) = 94%
8 CORIE	96 85		-40 -41 -42 -43 -44 -45 -46	40.8 - 42' LIMESTONE : BDX (LS), medium light gray (N6), strong to moderately fractured, slightly decomposed, narrow apertures. 42 - 58.9' SHALE : BDX (SH), medium gray (N5) to medium dark gray (N4), weathered, weak, thinly bedded, moderately to highly fractured.	BDX (LS)									RUN #8: Modified RQD = (81/85) = 94%
9 CORE	60 60		-47 -48 -49 -50 -51 -52	47.5' dark grayish brown (10YR 4/2), pale olive (5Y 6/4) discoloration, more competent. 50.2' weak to moderate. 50.8' olive gray (5Y 5/2).	BDX (SH)									RUN #9: Modified RQD = (52/60) = 87%



		1		Boring Number MW358	1	1					~ .		ge 4	of	5
Sar	nple	-							amp		Soil	Prope	erties		-
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well	Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
10 CORE	60 58		-53 -54 -55 -56 -57 -58	 42 - 58.9' SHALE: BDX (SH), medium gray (N5) to medium dark gray (N4), weathered, weak, thinly bedded, moderately to highly fractured. <i>(continued)</i> 52.2' dark grayish green (5GY 4/2). 54.1' medium dark gray (N4) to medium gray (N5), weak, highly decomposed, no visible bedding, dry. 55.7' dark grayish green (5GY 4/2). 57.2' light brownish gray (10YR 6/2), thinly bedded, laminated. 58.2' medium dark gray (N4), strong, intensely 	BDX (SH)										RUN #10: Modified RQD = (42/58) = 72%
11 CORE	36 31			fractured, thinly bedded. 58.9 - 64' LIMESTONE: BDX (LS), medium gray (N5), very strong, moderately fractured, visible laminations.	BDX (LS)										RUN #11: Modified RQD = (8/31) = 26%
12 CORIE	36 36			64 - 75.3' SHALE: BDX (SH), medium dark gray (N4) to medium gray (N5), strong, thinly bedded to											RUN #12: Modified RQD = (31/36) = 86%
13 CORE	48 48			laminated, moderately fractured. 64.3' grayish green (5GY 5/2), weathered, weak, decomposed.	BDX										RUN #13: Modified RQD = (43/48) = 90%
14 CORE	60 58			69.3' medium dark gray (N4), weathered, moderate strength.	(SH)										RUN# 14: Modified RQD = (57/58) = 99%



		1		Boring Number MW358		1			1			ge 5	of	5
	nple & (ii) # ⁽ⁱⁱ⁾	ınts	Feet	Soil/Rock Description And Geologic Origin For				PID 10.6 eV Lamp	sive (tsf)		Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Each Major Unit	USCS	Graphic Log	Well Diagram	PID 10.6	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
15	60		73	64 - 75.3' SHALE: BDX (SH), medium dark gray (N4) to medium gray (N5), strong, thinly bedded to laminated, moderately fractured. <i>(continued)</i>	BDX (SH)									RUN #15:
15 CORE	56			75.3 - 77.1' LIMESTONE: BDX (LS), gray (5Y 6/1), fossiliferous, very strong. 77.1 - 78.2' SHALE: BDX (SH), medium dark gray	BDX (LS)									Modified RQD = Not Recorded
			-78	 (N4), weathered, weak to moderate strength, moderately decomposed. 78.2 - 84.8' LIMESTONE: BDX (LS), medium dark gray (N4) to medium gray (N5), shaley, fossiliferous, very strong, moderately fractured, laminations (0-5%). 	BDX (SH)									
16 CORIE	60 51				BDX (LS)									RUN #16: Modified RQD = (23/51) = 45%
17 CORIE	60 60			84.8 - 90' SHALE : BDX (SH), dark gray (N3), weathered, weak to moderate strength, moderately decomposed, moderately fractured, thin bedding.	BDX (SH)									RUN #17: Modified RQD = (28/60) = 47%
L			-90	90' End of Boring.										



															ge 1	of	5
	ty/Proje dwin I			t	Li	cense/	Permit	Monito	oring l	Num	ber]	Boring	g Numl MW	^{ber} /392		
				of crew chief (first, last) and Firm	Da	te Dri	illing S	tarted]	Date I	Drilli	ng Co	mplete		Dril	ling Method
	ke We						0/0/	2022				C					
Cas	scade I	Drilli	ng	Common Well Name	Fi	nal Sta		2022 ter Lev	rel	Sur	ace E			2022	Bo		onic Diameter
				MW392			et (NA							AVD			.0 inches
				stimated: \Box) or Boring Location \boxtimes 0 N, 2,382,717.92 E E/(W)		La	ıt <u>38</u>	° 11	' 57	.132	" Loc	cal G	drid Lo	ocation			
State	1/4			/4 of Section , T N, R			g <u>-89</u>		. 0.				Fe]N]S		Feet W
Facili				County	State		<u> </u>	Civil T	own/C		_	lage			_~		
	1		1	Randolph	IL			Baldy	win				0.1	<u> </u>			
Sar	nple									DID 10 6 oV I cm			Soil	Prop	erties		-
	tt. & d (in	ints	Feet	Soil/Rock Description And Geologic Origin For						INC	ive -	tsf)					Ņ
ber Type	th A vere	Col	h In	Each Major Unit			C S	hic	ram	901	Dress	gth (ture ent	L g	icity (ment
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	5			U S O	Graphic Log	Well Diagram			Strength (tsf)	Moisture Content	Liquid	Plasticity Index	P 200	RQD/ Comments
1 CS	120 46		E	0 - 1.2' FILL, WELL-GRADED GRAVEL WIT CLAY: GW-GC, pinkish gray (7.5YR 6/2), an		or	(=111)	$b \cup C$			n m						CS= Core Sample
03	40			moist.	iyui	ai,	(FILL) GW-GC										
			- 1	1.2 - 16' FILL, LEAN CLAY: CL, light brown													Measured Rock
			-2	(7.5YR 6/4), sand (0-5%), no dilatancy, low t medium plasticity, moist.	to												Quality Designation
																	(RQD) was modified
			-3														due to
																	drilling methods,
			-4														modified RQD equals
			F														the sum of recovered
			-5														core sections
																	greater than 4 inches in
			<u>–</u> 6														length
			Ē				(FILL) CL										divided by total core
			7														recovery.
			-														
			-8														
			-9														
			F														
	100		-10														
2 CS	120 62																
			-11														
			E														
			-12														
	-	fy that	the inf	ormation on this form is true and correct to the l			y know	ledge.									
Signa	ture	5		- Firm Raml			74	541. 171		1	1	VT 5	2204		: (414)		
		100 million (1997)		234 W	v Fl	orida	Street, :								: (414)		DWIN 2022 GPL

234 W Florida Street, 5th Floor, Milwaukee, WI 53204 Fax: (414)837-3608 Template: RAMBOLL_IL_BORING LOG - Project: 845_BALDWIN_2022.GPJ



	1			Boring Number MW392	1		-			1	<u> </u>	1 ₽		ge 2	of	5
Number and Type	Length Att. & d Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well	Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)			Limit Limit	Plasticity sail.	P 200	RQD/ Comments
3 CS	120 33		$ \begin{array}{c} -13 \\ -14 \\ -15 \\ -16 \\ -17 \\ -18 \\ -19 \\ -20 \\ -21 \\ -22 \\ -23 \\ -24 \\ -25 \\ -26 \\ -27 \\ -28 \\ \end{array} $	 1.2 - 16' FILL, LEAN CLAY: CL, light brown (7.5YR 6/4), sand (0-5%), no dilatancy, low to medium plasticity, moist. <i>(continued)</i> 16 - 20' LEAN CLAY: CL, light brown (7.5YR 6/4), sand (0-5%), no dilatancy, low to medium plasticity, moist. 20 - 33' LEAN CLAY: CL, pinkish gray (7.5YR 6/2), sand (0-5%), medium to high plasticity, stiff, moist. 	(FILL) CL											
4 CS	120 104		-29 30 31 32	30' increasing sand and gravel content.												



				Boring Number MW392								ge 3	of	5
Sai	mple							dun		Soil	Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
5 CS	120 108		33 34 35 36 37 38 39 40 41 41 42 43 44 45 46 47	 20 - 33' LEAN CLAY: CL, pinkish gray (7.5YR 6/2), sand (0-5%), medium to high plasticity, stiff, moist. <i>(continued)</i> 33 - 35' WELL-GRADED SAND WITH SILT AND GRAVEL: (SW-SM)g, fine to medium sand, dry. 35 - 36.5' SANDY SILT WITH GRAVEL: s(ML)g, light yellowish brown (10YR 6/4), dry. 36.5 - 39' CLAYEY SILT: ML/CL, gray (7.5YR 5/1), sand (5-10%), coal (0-5%), gravel (0-5%), dry. 39 - 40' SILTY CLAY: CL/ML, sand (0-5%), low to medium plasticity, stiff. 40 - 48' SILT WITH SAND: (ML)s, light brownish gray (10YR 6/2), dry. 44' increasing clay content. 45' (2.5Y 6/2). 	CL (\$W-SM s(ML)g ML/CL CL/ML (ML)s									
6 CS	84 81		48 49 50 51 52	48 - 52' SILT: ML, gray (2.5Y 5/1), sand (0-5%), dry.	ML									



				Boring Number MW392								ge 4	of	5
Sar	nple							du		Soil	Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
			-	52 - 57' SHALE: BDX (SH), dark gray (5Y 4/1), highly weathered, hard, dry.										
			-53 -54	53' very dark gray (7.5YR 3/1).										
			-55		BDX (SH)									
			56											
7 Core	60 4		-58	57 - 57.5' LIMESTONE: BDX (LS), gray (5Y 6/1), slightly fractured. 57.5 - 70' SHALE: BDX (SH), dark gray (5Y 4/1), weathered, soft, moderately fractured to highly fractured limestone beds (0-5%).	BDX (LS)									RUN #7: Modified RQD = 0% (No Solid Recovery >
														4")
			61											
8 Core	96 78		-62											RUN #8: Modified RQD =
			-63 -64		BDX (SH)									(28/78) = 36%
			-65											
				66.3' - 67.2' highly fractured, very soft, wet.										
			68											
	100													
9 CORE	120 62		-71	70 - 74.4' LIMESTONE: BDX (LS), gray (5Y 6/1), moderately to intensely fractured, moderately wide apertures.	BDX (LS)									RUN #9: Modified RQD = (28/78) = 36%
	ļ		-72											



				Boring Number MW392								ge 5	of	5
Sam								amp		Soil	Prop	erties		-
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
10 CORE	48 48		-73 -74 -75 -76 -77 -78 -79 -80 -81 -82 -83 -84	70 - 74.4' LIMESTONE: BDX (LS), gray (5Y 6/1), moderately to intensely fractured, moderately wide apertures. <i>(continued)</i> 74.4 - 81.8' SHALE: BDX (SH), medium dark gray (N4) to dark gray (N3), slightly weathered, moderately fractured, thinly bedded. 81.8 - 84' LIMESTONE: BDX (LS), medium light gray (N6), shaley, fossiliferous, moderately fractured, thinly bedded. 83.2' medium gray (N5). 84' End of Boring.	BDX (LS) BDX (SH) BDX (LS)									RUN #10: Modified RQD = (28/48) = 58%



	/== .					·~ ·							ge 1	of	5
	ty/Proje dwin I			t	License	e/Permit	/Monit	oring I	Numbe	r	Boring	g Numl MW	ber 7393		
Borin	g Drille	d By:		of crew chief (first, last) and Firm	Date D	rilling S	tarted		Da	te Drill	ing Co			Dril	ling Method
	ke We cade l		na			Q/Q/	2022				10/4/2	2022		S	onic
	caue I		ng	Common Well Name	Final S			vel	Surfa	e Eleva		2022	Bo		e Diameter
	~ 11 ~			MW393	F	eet (NA	AVD8	(8)	43	4.59 F				6	.0 inches
				stimated: \Box) or Boring Location \boxtimes 7 N, 2,383,944.49 E E/(W)	L	.at _ 38	<u>8° 1</u> 1	<u>1' 57</u>	.027"	Local	Jrid Lo		N		
	1/4			/4 of Section , T N, R	Lo	ng <u>-89</u>	<u>0° 51</u>	<u>1'</u> <u>45.</u>							☐ E Feet ☐ W
Facili	ty ID				State		Civil T		City/ or	Village	e				
Sar	nple			Randolph	IL		Bald	Win	ط ط		Soil	Prop	erties		
	`		t	Soil/Rock Description					PID 10.6 eV Lamp						-
e	Att. 8 ed (i	ounts	ı Fee	And Geologic Origin For					5 eV	ssive (tsf)	0		~		nts
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Each Major Unit		CS	Graphic Log	Well Diagram	0.10.6	Compressive Strength (tsf)	Moisture Content	Liquid	Plasticity Index	200	RQD/ Comments
Nur and		Blo	Dep			U S	Grap Log	Well	PID	Cor Stre	C O	Liquid Limit	Plastic Index	P 2(
1 CS	120 86		E	0 - 1' FILL, WELL-GRADED GRAVEL: GW, pinkish gray (7.5YR 6/2), angular, moist.		(FILL) GW									CS= Core Sample
			1	1 - 20' FILL, LEAN CLAY: CL, brown (7.5YF	R 6/4),				Ϋ́Υ						Measured
			Ē	sand (0-5%), no dilatancy, low to medium pla moist.	asticity,										Rock Quality
			-2												Designation (RQD) was
			-3												modified due to
			F												drilling methods,
			E_4												modified RQD equals
															the sum of recovered
			-5												core
			-												sections greater than
			-6												4 inches in length
			E			(FILL) CL									divided by total core
			-7												recovery.
			Ē												
			<u>-8</u>												
			F o												
			-9												
			-10												
2 CS	120 120		-	10' sand (0-5%), iron concretions (0-5%).											
			-11												
			E												
<u> </u>			-12												
	•	fy that	the inf	ormation on this form is true and correct to the		ny know	ledge.								
Signa	ture	5		Firm Ram		<u> </u>	- 1 - F						: (414)		
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Template: RAMBOLL_IL_BORING LOG - Project: 845_BALDWIN_2022.GPJ



Sar	nple			Boring Number MW393					0.	1	Soil	ge 2 erties	of	5
Number and Type	t. & l (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well	Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)		ity	P 200	RQD/ Comments
			-13 -14 -15 -16 -17 -18 -19	 1 - 20' FILL, LEAN CLAY: CL, brown (7.5YR 6/4), sand (0-5%), no dilatancy, low to medium plasticity, moist. <i>(continued)</i> 18' medium to high plasticity. 	(FILL) CL									
3 CS	120 120		-20 -21 -22 -23	20 - 24' LEAN CLAY: CL, light brown (7.5YR 6/4), mottling, sand (0-5%), medium to high plasticity, cohesive, moist.	CL									
			-24 -25 -26	24 - 27' CLAYEY SAND: SC, gray (10YR 6/1), fine to medium sand, wet.	sc									
			-27 -28 -29 -30	27 - 31' SILT WITH SAND: (ML)s, dark gray (7.5YR 4/1), sand (0-5%), moist.	(ML)s									
4 CS	120 105		-31	30' coal fragments (0-5%). 31 - 40' SILTY CLAY: CL/ML, dark gray (7.5Y 4/1), organic material (0-5%), gravel (0-5%), stiff to very stiff, moist.	CL/ML									



				Boring Number MW393								age 3		5
Sar	nple							amp		Soi	l Pro	perties		-
	tt. & d (in)	ints	Feet	Soil/Rock Description And Geologic Origin For				eVL	ive tsf)					\$
ber Nype	th Al vered	Cou	h In l	Each Major Unit	CS	hic	mer	10.6	press gth (ture		t ícity ć		/ ment
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet		U S O	Graphic Loo	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture	Liquid	Limit Plasticity Index	P 200	RQD/ Comments
			-33	31 - 40' SILTY CLAY: CL/ML, dark gray (7.5Y 4/1), organic material (0-5%), gravel (0-5%), stiff to very stiff, moist. <i>(continued)</i>										
			-35											
			-36		CL/ML									
			-37											
			-38											
5 CS	120 120		-40	40 - 50' SILT: ML, grayish brown (2.5Y 5/2), very stiff to hard, platy, dry.										
			-41											
			-42											
			-43											
			-44											
			-45		ML									
			-46											
			-47											
			-48											
			-49											
6	120		50	50 - 55' SII T : MI dark grav (7 5YR 4/1) sand										
6 CS	92		-51	50 - 55' SILT: ML, dark gray (7.5YR 4/1), sand (0-5%), very stiff to hard, dry.	ML									
			-52											
			•		1	•		•	•				•	•



				Boring Number MW393							Pag	-	of	5
Sar	nple							amp			Prop	erties		-
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	SCS	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
ar N	ЦЩ.	B		50 - 55' SILT: ML, dark gray (7.5YR 4/1), sand	<u> </u>			[]	<u>0 2</u>	ΣŬ		PI	Ч	<u>2</u> 0
7 CORE	120 60		53 54 56 57 58 59 60 61 62 63 64 65 66 67 68 68	(0-5%), very stiff to hard, dry. <i>(continued)</i> 55 - 57' CLAYEY SILT : ML/CL, gray (10YR 6/1), sand (0-5%), gravel (0-5%), medium plasticity, moist. 57 - 60' LIMESTONE : BDX (LS), gray (10YR 6/1), rock flour and angular chips (<2"). 60 - 70' SHALE : BDX (SH), medium gray (N5), weathered, very weak, residual soil, soft, slightly fractured.	ML ML/CL BDX (LS) BDX (SH)									RUN #7: Modified RQD = (31/60) = 52%
8 CORIE	42 40		70	70 - 73.5' LIMESTONE: BDX (LS), medium dark gray (N4), weathered, shaley, thinly bedded, moderately fractured.	BDX (LS)			· · · · · · · · · · · · · · · · · · ·						RUN #8: Modified RQD = (32/40) = 80%



				Boring Number MW393	-			-				ge 5	of	5
San	nple							amp		Soil	Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
	Ц	H	-73	70 - 73.5' LIMESTONE: BDX (LS), medium dark gray (N4), weathered, shaley, thinly bedded, moderately fractured. <i>(continued)</i> 72' medium gray (N5).	BDX (LS)			H				H	H	
9 CORE	78 40			73.5 - 85' SHALE: BDX (SH), medium gray (N5), weathered, moderately to slightly fractured, thinly laminated.										RUN #9: Modified RQD = (30/40) = 75%
10 CORE	60 45			83.5' more competent. 85' End of Boring.	BDX (SH)									RUN #10: Modified RQD = (34/45) = 76%



													Pag		of	5
	ty/Proje dwin I			t		License/	Permit	/Monito	oring l	Number	r	Boring	g Numb MW	^{ber} 7394		
				of crew chief (first, last) and Firm		Date Dri	illing S	tarted		Da	te Drill	ing Co			Dril	ling Method
	ke We scade l		na				0/25	/2022				10/5/2	2022		S	onic
	scaue I	JIIII	ng	Common We	ell Name	Final Sta			el	Surfac	e Eleva		2022	Bo		e Diameter
				MWS		Fe	et (NA	AVD8	8)		5.51 Fe	,		/	6	.0 inches
				stimated: \Box) or Boring Location 3 N, 2,385,095.76 E E/(V		La	nt <u>38</u>	<u>8° 11</u>	<u>' 56.</u>	<u>8911"</u>	Local (Grid Lo				
21410	1/4	-		/4 of Section , T N, R	-	Lon	g <u>-89</u>	<u>9° 51</u>	<u>' 31.</u>	1756"		Fe]N]S		□ E Feet □ W
Facili	ty ID			County	S	tate	-	Civil T		City/ or	Village	•				
	n n 1 n			Randolph	1	L		Baldy	<i>v</i> ın			Sail	Prop	antiaa		
Sai	nple			Soil/Rock Descripti	an					PID 10.6 eV Lamp						_
	Length Att. & Recovered (in)	unts	Depth In Feet	And Geologic Origin						eV]	sive (tsf)					ts
lber Type	gth A overe	Blow Counts	h In	Each Major Unit			CS	hic	ram	10.6	pres	sture	t, iq	icity x	0	RQD/ Comments
Number and Type	Length Att. & Recovered (in)	Blow	Dept				U S I	Graphic Log	Well Diagram		Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comr
1 CS	72 67		-	0 - 2.6' FILL, WELL-GRADED GR, CLAY: GW-GC, brown (10YR 4/3),						\$						CS= Core Sample
00	07				angular, i	10101.										
							(FILL) GW-G0									Measured Rock
			-2													Quality Designation
			E					000								(RQĎ) was
			-3	2.6 - 20' LEAN CLAY: CL, brown (reddish brown bottling (20%), sand	10YR 5/3)	, w to										modified due to
				medium plasticity, very stiff to hard	, moist.						4					drilling methods,
			-4													modified RQD equals
																the sum of recovered
			-5								4					core
											4					sections greater than
2	120		-6													4 inches in length
2 CS	120		-								2.5					divided by total core
			-7								2.0					recovery.
			-				CL				3.5					
			-8													
											2					
			-9	9.2' brown (7.5YR 5/3), medium to	high place	ticity										
			-	9.2 brown (7.51K 5/5), medium to	nigir pias	ucity.					2					
			$\frac{-10}{2}$													
			-								3					
			11 													
			-12								2.25					
	bv certi	fy that		ormation on this form is true and corr	ect to the b	pest of m	v know	ledge					1	1		<u> </u>
Signa	-		ine mi		^{rm} Ramb		,						Tel	: (414)	837-3	607
	4	2	-	- gru		Florida S							Fax	: (414)	837-3	608
							Т	emplate:	RAM	BOLL	IL_BOR	ING LO	OG - Pro	oject: 84:	5_BAL	DWIN_2022.GPJ



				Boring Number MW394								ge 2	of	5
San	nple							dup		Soil	Prope	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
3 CS	120 120		13 14 15 16 17 18 19 20	 2.6 - 20' LEAN CLAY: CL, brown (10YR 5/3), reddish brown bottling (20%), sand (0-5%), low to medium plasticity, very stiff to hard, moist. <i>(continued)</i> 14' low to medium plasticity. 16.5' increasing sand and gravel content, gray (GLEY 1 5/1) iron concretions (50%). 	CL				2.25					
4 CS	120 112		$ \begin{array}{c} 20 \\ -21 \\ -22 \\ -23 \\ -24 \\ -25 \\ -26 \\ -27 \\ -28 \\ -29 \\ -30 \\ -31 \\ -32 \\ -32 \\ \end{array} $	20 - 22.1' SILTY SAND: SM, yellowish brown (10YR 5/6), fine sand, clay (0-5%), moist. 22.1 - 36.8' LEAN CLAY: CL, dark yellowish brown (10YR 4/4), greenish gray (GLEY 1 5/10Y) and yellowish brown (10YR 5/6) mottling, sand (0-5%), medium to high plasticity, hard, moist.	SM				 4.5 					

MW204



6 96 46 36.8 - 48 Weethered SHALE Bodrock: BDX (SH), pale olive (5Y 6/3), weathered, argillaceous, fissile, moist. 3.75 6 96 46 47 48 59 'LIMESTONE: to SHALE: BDX (LS), olive gray (5Y 5/2). 80X (SH)					Boring Number MW394									ge 3	of	5
6 96 96 42-1-36.8 LEAN CLAY: CL, dark yellowish provi (10YR 44), presink prov (LCY 15/10Y) and yellowish brown (10YR 566) motting, sand (<i>Continued</i>) 3.75 33 4.55 4.25 34 34.4 olive yellow (5Y 6/6), low to medium plasticity. (<i>Continued</i>) 0. 34 34.4 olive yellow (5Y 6/6), low to medium plasticity. (<i>Continued</i>) 0. 35 113 36.8 - 49' Weathered SHALE Bedrock: EDX (SH), pale olive (5Y 5/3), weathered, argillaceous, fissile, moist. 4.5 40 40' olive gray (5Y 5/2). 40' olive gray (5Y 5/2). 80X (SH) 41 44 44 80X (SH) 80X (SH) 43 44 44 80X (SH) 80X (SH) 44 43 44 44 44 44 44 44 44 44 44 44 44 44 44 44 45 46 47 48 46 47 48 44 44 46 48 44 44 44 47 48 48<	Sar									amp		Soil	Prop	erties		
6 96 46 96 46 96 47 48 59: UMESTONE: to SHALE: BDX (LS), olive gray (5Y 5/2). 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS) (LS), olive gray (SY 4/2), interbedded imestone and shale. 80X (LS),	Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	And Geologic Origin For	SC	Graphic Log	Well	Diagram	PID 10.6 eV Lá	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
6 96 40° olive gray (5Y 5/2). 96 44 43 44 44 45 46 96 47 48 48 - 58' LIMESTONE: to SHALE: BDX (LS), olive gray (5Y 4/2), interbedded limestone and shale, fissile.					brown (10YR 4/4), greenish gray (GLEY 1 5/10Y) and yellowish brown (10YR 5/6) mottling, sand (0-5%), medium to high plasticity, hard, moist. <i>(continued)</i> 34.4' olive yellow (5Y 6/6), low to medium plasticity. 36.8 - 48' Weathered SHALE Bedrock: BDX (SH), pale olive (5Y 6/3), weathered, argillaceous, fissile,						3.75 4.25					
50' - 50.2' limestone, very strong.	6 CS	96 96		40 41 42 43 44 45 46 47 48	48 - 58' LIMESTONE: to SHALE: BDX (LS), olive gray (5Y 4/2), interbedded limestone and shale, fissile.	(SH)										
50' - 50.2' limestone, very strong.				-51	50' - 50.2' limestone, very strong.	BDX (LS)										



				Boring Number MW394							Pag	ge 4	of	5
San	nple							dur		Soil	Prope	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diaoram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
7 CS	48 48			 48 - 58' LIMESTONE: to SHALE: BDX (LS), olive gray (5Y 4/2), interbedded limestone and shale, fissile. <i>(continued)</i> 53.7' - 53.9' limestone, very strong. 54' - 55.6' dark gray (10YR 4/1) to gray (10YR 5/1), more competent. 55.6' gray (10YR 6/1) to dark gray (10YR 4/1), more competent. 	BDX (LS)									
8 CORE	18 14			58 - 59.7' LIMESTONE: BDX (LS), medium gray (N5), shaley, laminated, moderately fractured.	BDX (LS)									RUN #8: Modified RQD = (4/14) = 29%
9 CORE	60 60		60 61 62 63 64	59.7 - 68' SHALE : BDX (SH), medium dark gray (N4), weathered, very weak to weak, thinly bedded, moderately fractured.	BDX (SH)									RUN #9: Modified RQD = (48/60) = 80%
10 CORIE	57 56		-65 -66 -67	64.5 - 67.2' highly decomposed, weathered, wet.										RUN #10: Modified RQD = Not Recorded
11 CORE	68 68			68 - 68.4' LIMESTONE: BDX (LS), light olive gray (5Y 6/2) to olive gray (5/2). 68.4 - 70.8' SHALE: BDX (SH), medium dark gray (N4), weathered, very weak to weak, thinly bedded, moderately fractured.	BDX (LS) BDX (SH) BDX									RUN #11: Modified RQD = (42/68) = 62%
			-72	71 - 77.6' SHALE: BDX (SH), dark gray (N3),	(LS)			-1. -						



				Boring Number MW394								ge 5	of	5
San	nple							amp		Soil	Prope	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
12 CORE	60 59		-73 -74 -75 -76 -77	strong, thinly bedded, moderately fractured. 71 - 77.6 SHALE: BDX (SH), dark gray (N3), strong, thinly bedded, moderately fractured. <i>(continued)</i>	BDX (SH)								1	RUN #12: Modified RQD = (44/59) = 75%
13 CORIE	60 48		- 78 - 79 - 80 - 81 - 82	 77.6 - 80' LIMESTONE: BDX (LS), medium gray (N5), shaley, weak, moderately fractured. 80 - 85' SHALE: BDX (SH), medium dark gray (N4), weathered, weak, thinly bedded, moderately fractured, moist to wet. 	BDX (LS)									RUN #13: Modified RQD = (40/48) = 83%
				85' End of Boring.	BDX (SH)									



-	y/Proje			nnlav	License/	Permit	Monito	oring l	Number		Boring				
Boring	g Drille	d By:	gy Cor Name c	of crew chief (first, last) and Firm	Date Dri	lling St	tarted		D	ate Drilli	ing Cor			Dril	ling Method
-	rk Ba	-				U					U	1			1/4 HSA
	ldog l		ng)/2015				11/24/	2015		an	d rotary
				Common Well Name						ce Eleva					Diameter
ocal	Grid O	rigin		MW-370 stimated:) or Boring Location	Fe	et (NA	AVD8	8)	41	8.67 F	eet (N Grid Lo		38)	8	.3 inches
				50 N, 2,381,936.14 E E/W	La	.t <u>38</u>	<u> 1</u>	<u>1'</u> <u>44</u>	.1702 "	Local			N		
	1/4			1/4 of Section , T N, R	Lon	g <u>-89</u>	<u>)° 52</u>	<u>2' 10</u>	.8084"		Fe]S		Feet
Facilit				County	State	<u></u>	Civil T		City/ or	Village					
				Randolph	Illinois		Bald	win							
San	nple										Soil	Prope	erties		_
	k (ii)	ts	set	Soil/Rock Description						e (j					
л е.	Att. red	oun	n Fe	And Geologic Origin For		s			=	essiv h (ts	e 1		ty		ents
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Each Major Unit		U	Graphic Log		Diagram	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	00	RQD/ Comments
Nur and	Ler Rec	Blo	Del			U S	Grap Log	Well		Co1 Stre	C OI	Liquic Limit	Plastic Index	P 200	RQ Coi
			-	0 - 2' SILTY CLAY CL/ML.				\mathbb{N}	×						0-28' Blind Drilled. Se
			È.						X						log PZ-17
			-1			CL/ML									for soil descriptio
			E												lacscriptio
			-2	2 - 4' Shelby Tube Sample.		<u></u>	<u> </u>								
			F												
			-3												
			F												
			E	L		L									
			Ę	4 - 8' SILTY CLAY CL/ML.											
			È_												
			-5												
			F												
			-6			CL/ML									
			E			-									
			-7												
			F												
			F o												
			-8	8 - 10' SILTY CLAY to LEAN CLAY: CL/	ML.										
			E												
			-9			CL/ML									
			F												
			-10	10 - 12' LEAN CLAY: CL.		<u></u>									
			E												
			E_11			_									
						CL									
			È 12												
			-12				1 / /								

Signature	Firm Natural Resource Technology 234 W. Florida St., Fifth Floor, Milwaukee, WI 53204	Tel: (414) 837-3607 Fax: (414) 837-3608
		G LOG - Project: BALDWIN GINT.GPJ



			TEC	HNOLOGY Boring Number MW-370						Pa	ge 2	of	4
San	nple								Soil	Prop			_
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
			-	12 - 14' Shelby Tube Sample.									
			-13 -14 -15 -16 -17 -18 -19 -20 -21 -22 -22 -23	- 14 - 24' SILTY CLAY CL/ML.	CL/ML								
			-24										
			-25 -26 -27	26 - 28' SILTY CLAY CL/ML.									
1 SS 1 CORE	10 10 60 18.5	23 50/4"	-28 -29 -30 -31 -32	28 - 28.4' LEAN CLAY: CL, yellowish brown (10YR 5/4), trace angular limestone gravel, soft, medium plasticity, moist. 28.4 - 28.9' SHALE: BDX (SH), gray, highly decomposed, very weak. 28.9 - 38.1' SHALEY LIMESTONE: BDX (LS/SH), light gray to gray, intensely fractured (extremely narrow to moderately narrow apertures), medium to thickly bedded, microcrystalline, moderately decomposed, very strong.	BDX (LS/SH								Core 1, RQD=51%



			TEC	HNOLOGY										
				Boring Number MW-370		1					Pag		of	4
San	nple									Soil	Prop	erties		_
	Length Att. & Recovered (in)	its	eet	Soil/Rock Description					sf)					
r pe	l Att ered	Cour	In F	And Geologic Origin For	s	2		E	essi ^r th (t	t Ie		ity		ents
Number and Type	Length Att. & Recovered (in	Blow Counts	Depth In Feet	Each Major Unit	SC	Graphic Log	Well	agra	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	200	RQD/ Comments
an	Le Re	Bl	De		5	Grap	Š	Ä	Str Co	žů	ĒĒ	Pla Inc	Р	Co R
			-33	28.9 - 38.1' SHALEY LIMESTONE : BDX (LS/SH), light gray to gray, intensely fractured (extremely narrow to moderately narrow apertures), medium to thickly bedded, microcrystalline, moderately decomposed, very strong. <i>(continued)</i>			I I I							
2 CORE	51.5 12		-34	33.9' - 38.1' gray, greenish gray in fractures, trace fossils, moderately to highly decomposed, slightly to moderately disintegrated, clay in shoe with a hard, reddish brown inclusion.	BDX (LS/SH									Core 2, RQD=0%
			36 	36' - 37.9' vertical fracture.			I I I							
			E_38				Ι							
3 CORE	24 25		-39	38.1 - 44' SHALE : BDX (SH), bluish gray, intensely fractured (extremely narrow to narrow apertures), highly decomposed, weak.										Core 3, RQD=40%
			-40											
4	24		- 40											Core 4,
CORE	11		-41	40.6' - 40.8 shaley limestone layer, light gray to										RQD=0%
5	36		- 41	gray, microcrystalline, moderately decomposed, very strong.	BDX (SH)									Core 5,
CORE	32		-42	41.1' - 43.2 gray, moderately to highly decomposed.										RQD=78%
-			- 42											
			-43											
			4 3											
			F 14											
6 CORE	12 28		-44	44 - 45.7' SHALEY LIMESTONE: BDX (LS/SH), light gray to gray, intensely fractured (extremely			1							Core 6, RQD=29%
0011	20		-45	narrow to narrow apertures), thin to medium	BDX									
7	45		4 3	bedded, microcrystalline, slightly decomposed, clay cement in apertures, very strong.	(LS/SH									Core 7,
7 CORE	27		-46	45' shale layer, bluish gray, moderately fractured (extremely narrow to narrow apertures), highly	<u>+</u>		1							RQD=65%
			-40	decomposed, weak.										
			-47	45.7 - 52.2' SHALE: BDX (SH), bluish gray, moderately fractured (tight to narrow), highly										
			F ⁴ /	decomposed, weak.										
			- 40											
			48											
			È .a		BDX									
8	24		-49 -		(SH)									Core 8,
CORE	30		=											RQD=78%
			50											
			╞ <i>~</i> .											
LL 	24		51											Cara
9 CORE	24 24		= 50											Core 9, RQD=0%
-	1		-52	1	I		ľ.				I			



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~				Boring Number MW-370		1	1		~	Pag		of	4
San	nple								Soil	Prope	erties		4
	& (ii)	ts	set	Soil/Rock Description				ve (f)					
r g	Att. red	Joun	n Fe	And Geologic Origin For	s	0	В	essiv h (ts	t e		ty		ents
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Each Major Unit	SCS	Graphic Log	Well Diagram	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	00	RQD/ Comments
Nu and	Leı Re	Blc	De		ñ	Grap Log	Well Diagr	Co: Str	C ₀ Mc	Liquid Limit	Plastic Index	P 200	Co RC
			F	<u>52' clay cement.</u> <u>52.2 - 61.7' SHALEY LIMESTONE:</u> BDX (LS/SH),	+								
			-53	light gray to gray, intensely fractured (very narrow to									
10	24		- 55	narrow), thin to medium bedded, microcrystalline, slightly decomposed, cemented clay in apertures,			1 目:						Core 10,
10 CORE	36		-	very strong. 52.7' - 53' clayey sand in aperture.			1 目						RQD=0%
			-54	53' - 53.1 shale bed, bluish gray, fossiliferous,			1 目:						
				moderately fractured (very narrow to narrow), highly decomposed, weak.									
			-55	53.1' white to bluish gray, gray in the fractures			1 目:						
11 🗖	24		_	(extremely narrow to moderately narrow apertures), thinly to medium bedded, slightly to moderately									Core 11,
11 CORE	30		-56	disintegrated. 55.7' moderately disintegrated.			1 目:						RQD=18%
			Ē										
			-57		BDX (LS/SH	╞╧╧							
			F		ſ								
12	30		-58	58.1' highly decomposed.									Core 12,
12 CORE	27		-	30.1 mgmy decomposed.			1:目:						RQD=39%
			-59				目						
			-										
			-60				1:目:						
			F				1:目:						
13 CORE	36		-61										Core 13,
CORE	53		-] 目:						RQD=89%
			-62	61.7 - 65.3' LIMESTONE: BDX (LS).] 目:						
			Ē										
			-63										
			_		BDX								
			-64		(LS)								
			-65										
			E	65.3 - 66' Overdrilled for Well Installation.									
			-66										
				66' End of Boring.									Bedrock corehole
													reamed 6" in diameter
													to 66' for
													well installation.
			I			I							



				INOLOGI								Pag		of	2		
	ty/Projec		ne y Com	nlav	License/	Permit/	Monito	oring N	lumbe	r	Boring	Numb PZ-1					
				f crew chief (first, last) and Firm	Date Dri	illing St	arted		E	ate Drilli				Dril	ling Method		
Ch	ad Dut	ton				Ū.					-	-			ollow stem		
Bu	ldog [Drillii	ng		F' 10	7/29/2015 7/29/2015 Final Static Water Level Surface Elevation								auger			
				Common Well Name PZ-170		atic Wat eet (NA				ice Eleva 18.58 Fo				Borehole Diameter 8.3 inches			
Local	Grid Oı	rigin	(es	stimated:) or Boring Location		<u> </u>		/		Local (,0)				
State	Plane	556	5,822.6	9 N, 2,381,944.92 E Е/🛞	La	at <u>38</u>		<u>1' 44</u>		-			N		E		
E- ili	1/4	of	1	/4 of Section , T N, R	Lon			<u>2' 10.</u>		<u>'</u> Village	Fe	et 🗌	S		Feet W		
Facili	IJD			5	State Illinois		Bald		ny/ or	village							
Sar	nple										Soil	Prope	erties				
	k (iii	s	ज ज	Soil/Rock Description													
, e		Blow Counts	Depth In Feet	And Geologic Origin For					_	Compressive Strength (tsf)	e		_N		nts		
Number and Type	Length Att. Recovered (C A	th L	Each Major Unit		CS	Graphic Log	Well		npre	Moisture Content	Liquid Limit	Plasticity Index	8	RQD/ Comments		
Nun and		Blo	Dep			N S	Graf Log	Well		Cor Stre	Mo Cor	Liquic Limit	Plastic Index	P 200	RQ Cor		
1 SS	24 8	4 5 6 9	F	0 - 2' SILTY CLAY CL/ML, yellowish brown (5/6), trace brown (10YR 5/3) and very dark br	(10YR rown				8								
		9	E1	(10YR 2/2) mottling, silt (15-25%), trace roots gravel, and coarse sand, cohesive, nonplastic	, grass,	CL/ML											
				plasticity, hard (>4.5 tsf), dry.	, 10 10 10												
2	24		-2	2 - 4' Shelby Tube Sample.											ST2: 24"		
ST	21		E												push at 500lbs of		
			-3												pressure.		
			Ē,														
3 SS	24 15	2 3 5 7	<u>–</u> 4	4 - 8' SILTY CLAY CL/ML, yellowish brown (5/6), trace brown (10YR 5/3) and very dark br	(10YR												
33	15	5 7	5	(10YR 2/2) mottling, silt (5-15%), trace very fir	ne sand												
			E	and gravel, low plasticity, very stiff to hard (2. tsf), dry.	5->4.5												
	24	3	-6	$C_{1} = 7.41$ trace grow (10)/D E(1) mettling		CL/ML											
ss	24 17	3 5 8		6' - 7.4' trace gray (10YR 5/1) mottling.													
		8	-7														
	V		E														
5	24	3	-8	8 - 10' SILTY CLAY to LEAN CLAY: CL/ML													
SS	17	3 4 6 6	Ē	yellowish brown (10YR 5/6), trace brown (10) and very dark brown (10YR 2/2) mottling, silt	/R 5/3)												
/			-9	(5-15%), trace very fine sand and gravel, silt of decreases with depth, clay content increases		CL/ML											
			-10	depth, medium plasticity, very stiff (3.25 tsf), o	dry												
6 SS	24 20	3 4 5 5	- 10	10 - 12' LEAN CLAY: CL, brown (5YR 4/3), 1 very dark brown (10YR 2/2) mottling, trace sil	trace t. silt												
		5	-11	content increasing with depth, medium to high plasticity, stiff (1.75-2.0 tsf).		CL											
			Ē												ST7: 24"		
7	24		-12	12 - 14' Shelby Tube Sample.											push at		
ŚT	24		È												250lbs of pressure.		
			-13				<u> </u>										
I here Signa		ty that	t the info	bring on this form is true and correct to the be			•										
Siglia	fill fill	An	N	hold Firm Natur 234 W	ral Reso 7. Florida					e. WI 532	204			837-30 837-30			

 234 W. Florida St., Fifth Floor, Milwaukee, WI 53204
 Fax: (414) 837-3608

 Template: ILLINOIS BORING LOG - Project: BALDWIN GINT.GPJ



			TEC	HNOLOGY Boring Number PZ-170						Pa	ge 2	of	2
San	nple								Soil	Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
				12 - 14' Shelby Tube Sample. (continued)									
8 SS	24 21	3 5 7 8	-14	14 - 24' SILTY CLAY CL/ML, yellowish brown (10YR 5/6), trace brown (10YR 5/3) and very dark brown (10YR 2/2) mottling, silt (10-20%), trace gravel, cohesive, low plasticity, stiff to very stiff (1.0-3.0 tsf), dry to moist. 14.9' - 15.3' very dark brown (10YR 2/2) mottling.									
9 SS	24 24	2 4 6		16' - 18.5' increaed very dark brown (10YR 2/2) mottling (5-15%), very fine sand (0-10%), trace fine gravel, subangular, cohesive, low to medium plasticity, dry to moist. 16.8' - 17.1' very dark brown (10YR 2/2) mottling.									
10 SS	24 24	1 3 3 3	-18	 18' - 20' silt (15-25%), very fine sand (0-10%), trace fine gravel, medium plasticity, moist. 19' layer of gravel (2" thick, subangular to 	CL/ML								
11 SS	24 20	1 2 5 7	20	subrounded). 19.8' very soft (0.25 tsf). 20' - 24' subangular to subrounded gravel, low plasticity, dry to moist. 20.8' increased gravel content (10-15%). 21.2' decrease in gravel content (5-15%).									
12 SS	24 20.5	3 6 8 10	-22										
13 ST	24 24		-24	24 - 26' Shelby Tube Sample.									ST13: 24" push at 650lbs of pressure.
14 SS	24 22	3 6 12 14	-26	26 - 28.2' SILTY CLAY CL/ML, yellowish brown (10YR 5/6), trace brown (10YR 5/3) and very dark brown (10YR 2/2) mottling, silt (10-30%), very fine sand (0-15%), trace fine subangular to subrounded gravel, gravel decreases with depth to no gravel, trace <1mm thick very fine sand seams, cohesive,									
15 SS	24 22	9 17 24 35	-28	low to medium plasticity, plasticity increasing with depth, very stiff to hard (2.0->4.5 tsf), moist, // decreasing silt and sand content with depth. // 28.2 - 30 LEAN CLAY: CL, very dark gray (2.5Y 3/1), trace silt, cohesive, medium to high plasticity, hard (>4.5 tsf), dry.	CL								
16 SS	17 13	11 30 50 for 5"	-30	nard (>4.5 tst), dry. 28.5' black (2.5Y 2.5/1). 28.9' greenish gray (GLEY 1 6/1). 30 - 31.1' SHALE: to LEAN CLAY: BDX (SH), greenish gray (GLEY 1 6/1), trace silt, cohesive, medium to high plasticity, dry, shale (residual soil to highly decomposed, very weak, fissile). 31.1' End of Boring.	BDX (SH)								Hollow Stem Auger Refusal at 31.1 ft bgs on Shale Bedrock.



MONITORING WELL CONSTRUCTION

Facility/Project Name	Local Grid Location of Well		Well Name	
Baldwin Energy Complex	t. □ N. S. Local Grid Origin □ (estimated: □	$\underbrace{\Box}_{ft} \underbrace{\Box}_{W} \underbrace{E}_{t}$		
Facility License, Permit or Monitoring No.				
	Lat. <u>38°</u> <u>11'</u> <u>44.170"</u> Long.	<u>89°</u> <u>52'</u> <u>10.808"</u> or	MW-370	
Facility ID	St. Plane556,826.50ft. N,,2	381,936.14 ft. E. E/Ŵ	Date Well Installed	
	Section Location of Waste/Source	0	11/25/2015	
Type of Well	1/4 of 1/4 of Sec		Well Installed By: (Person's Name and Firm)	Į.
mw	Location of Well Relative to Waste/Sou	Irce Gov. Lot Number	Mark Baetje	
Distance from Waste/ State	u 🗆 Upgradient s 🗆 Side	gradient		
ft. Illinois	d 🛛 Downgradient 🛛 n 🗆 Not			_
A. Protective pipe, top elevation	ft. (NAVD 88)	1. Cap and lock?	⊠ Yes □ No	
B. Well casing, top elevation 42	20.85 ft. (NAVD88)	2. Protective cover pa a. Inside diameter:	<u>4.0</u> ii	in.
C. Land surface elevation4	18.67 ft. (NAVD88)	b. Length:	5.0 f	ft.
D. Surface seal, bottom ft. (NA	VD88).or ^{1.0} ft.	c. Material:	Steel 🛛 Other 🗆	
12. USCS classification of soil near screen:			ection? 🛛 🖾 Yes 🗆 No)
		If yes, describe:	Three steel bollards	
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		3. Surface seal:	Bentonite □ Concrete ⊠	
13. Sieve analysis attached? \Box Ye	es 🛛 No		Other	
14. Drilling method used: Rotat	v 🖂 🔰 👹 👹		well casing and protective pipe:	
Hollow Stem Aug			Bentonite 🖂	
-	er 🗆 🛛 🕅 🕅		Sand Other 🛛	
		5. Annular space sea	l: a. Granular/Chipped Bentonite	
6	ir 🗆 🛛 👹 👹		ud weight Bentonite-sand slurry	
Drilling Mud $\Box 0.3$ Nor	ne 🗆 🛛 🗮 👹	cLbs/gal m	ud weight Bentonite slurry	
16. Drilling additives used?			ite Bentonite-cement grout 🛛	
			volume added for any of the above	
Describe		f. How installed:		
17. Source of water (attach analysis, if required			Tremie pumped	
			Gravity 🗆	
Village of Baldwin		6. Bentonite seal:	a. Bentonite granules	
E. Bentonite seal, top	(D88) or 29.0 ft.		$3/8$ in. \Box $1/2$ in. Bentonite chips \boxtimes Other \Box	
			: Manufacturer, product name & mesh size	
F. Fine sand, top ft. (NAV		a b. Volume added	ft ³	
G. Filter pack, top ft. (NAV	D88) or 51.0 ft.	8. Filter pack materia	al: Manufacturer, product name & mesh size	
H. Screen joint, top 365.7 ft. (NAV	'D88) or 53.0 ft.	a. <u>Unin</u> b. Volume added	nin Corporation, FILTERSIL	
		9. Well casing:	Flush threaded PVC schedule 40 \boxtimes	
I. Well bottom ft. (NAV	D88).or 63.0 ft.	9. Wen easing.	Flush threaded PVC schedule 80	
255.0	D88) or 63.5 ft.	<	Other Other	
J. Filter pack, bottom ft. (NAV	(D88) or 63.5 ft.	10. Screen material: a. Screen Type:	Schedule 40 PVC Factory cut	
K. Borehole, bottom <u>352.7</u> ft. (NAV	/D88) or 66.0 ft.	a. Screen Type.	Continuous slot	
			Other	
L. Borehole, diameter <u>6.0</u> in.		b. Manufacturer		
		c. Slot size:	<u> </u>	in.
M. O.D. well casing 2.38 in.		d. Slotted length:	<u>10.0</u> f	ft.
2.07		11. Backfill material (below filter pack): None \Box os, 0.4' of bedrock drill cuttings Other \boxtimes	
N. I.D. well casing 2.07 in.		2.1 of bentonne chi	55, 0.7 Of Decidence unit cutings Other 🛛	
I haraby cartify that the information on this form	a is true and correct to the best of my lim	owladaa	Date Modified: 2/26/2016	—
I hereby certify that the information on this form	Firm Natural Resou	-	Tel: (414) 837-3607	—

ignature	Brad Ruches	Firm Natural Resource Technology 234 W. Florida Street, Floor 5, Milwaukee, WI 53204	Tel: (414) 837-3607 Fax: (414) 837-3608

	Incorporated						DBEHOLE TPZ-164 (Page 1 of 1)							
F	Phase II Hydrogeologic Investigation Baldwin Energy Complex Dynegy Midwest Generation, Inc.	Date Completed : 08/26/2013 Hole Diameter : 8 1/2" OD / 4 1/4" ID Drilling Method : HSA (CME-55LC) Sampling Method : Split Spoon / Shelby Tube Drilling Company : Bulldog Drilling, LLC							Driller : John Gates Geologist : Stuart Cravens (Ki Ground Elevation : 432.50 Casing (MP) Elevation : 435.10 X,Y Coordinates : 2383909, 556829					
Depth in Feet	DESCRIPTION		Surf. Elev. 432.50	Samples	Blow Count	Recovery inches	Qp TSF	nscs	GRAPHIC	Well: TI Elev.: 4				
0- - - 1-	FILL - Bottom Ash, coarse, black (10YR 2	/1), dry									- Concrete			
2-	- - - - moist - Shelby Tube Sample ST164-5 @ 3-5 grain size analysis (Ash):	'>	- 430								[—] Seal Bentonite Chips [—] Riser (Sch 40 PVC)			
4- 5-	- wet		- 429 - 428	1		17/24		AR						
6-			- 427 - 426											
7-			- 425								— Filter Pack — Screen (pre-pack) 2"ID/3.5"OD; 4.50' ope			
9-	CLAY (lean), stiff, medium to high plasticit (10YR 4/1), moist - @8.9' - light yellowish brown (10YR 6 light gray mottling - @9.3' - gray (10YR 6/1) with 25-50% brownish-yellow mottling (10YR 6/6)	6/4) with <10%	- 424 - 423	2	3 3 5	18/18		CL			— Bottom Cap			
11-	- light olive brown <shelby 10<br="" @="" sample="" st164-12="" tube="">grain size analysis: 7.2% Sand, 62.2% Silt, 30.6% Clay</shelby>)-12'>	- 422	3		23/24		CL			Seal Bentonite Chips			

- 420

- 419

	Incorporated						DBEHOLE TPZ-164 (Page 1 of 1)							
F	Phase II Hydrogeologic Investigation Baldwin Energy Complex Dynegy Midwest Generation, Inc.	Date Completed : 08/26/2013 Hole Diameter : 8 1/2" OD / 4 1/4" ID Drilling Method : HSA (CME-55LC) Sampling Method : Split Spoon / Shelby Tube Drilling Company : Bulldog Drilling, LLC							Driller : John Gates Geologist : Stuart Cravens (Ki Ground Elevation : 432.50 Casing (MP) Elevation : 435.10 X,Y Coordinates : 2383909, 556829					
Depth in Feet	DESCRIPTION		Surf. Elev. 432.50	Samples	Blow Count	Recovery inches	Qp TSF	nscs	GRAPHIC	Well: TI Elev.: 4				
0- - - 1-	FILL - Bottom Ash, coarse, black (10YR 2	/1), dry									- Concrete			
2-	- - - - moist - Shelby Tube Sample ST164-5 @ 3-5 grain size analysis (Ash):	'>	- 430								[—] Seal Bentonite Chips [—] Riser (Sch 40 PVC)			
4- 5-	- wet		- 429 - 428	1		17/24		AR						
6-			- 427 - 426											
7-			- 425								— Filter Pack — Screen (pre-pack) 2"ID/3.5"OD; 4.50' ope			
9-	CLAY (lean), stiff, medium to high plasticit (10YR 4/1), moist - @8.9' - light yellowish brown (10YR 6 light gray mottling - @9.3' - gray (10YR 6/1) with 25-50% brownish-yellow mottling (10YR 6/6)	6/4) with <10%	- 424 - 423	2	3 3 5	18/18		CL			— Bottom Cap			
11-	- light olive brown <shelby 10<br="" @="" sample="" st164-12="" tube="">grain size analysis: 7.2% Sand, 62.2% Silt, 30.6% Clay</shelby>)-12'>	- 422	3		23/24		CL			Seal Bentonite Chips			

- 420

- 419



Facili	ty/Proje	ot Nor	<u></u>		Liconso	Dormit	Monit	oring	Jumbo	*	Boring		ge 1	of	2		
	dwin I			ıt	License/Permit/Monitoring Number						DOULLE						
Borin	g Drille	d By:	Name	of crew chief (first, last) and Firm	Date Drilling Started Date Dr					ate Drilling Completed					ling Method		
	en Litt				9/23/2022					0/02/0000					Sonia		
	scade I	Jriin	ng	Common Well Name	Final Sta				Surfac	e Eleva	9/23/2022 evation Box				Sonic rehole Diameter		
				XPW01		et (NA				5.12 F		AVD			6.0 inches		
				stimated:) or Boring Location		at <u>38</u>	3° 11	1' 51.0	807"	Local	Grid Lo						
State	Plane 1/4			8 N, 2,383,427.03 E E/() //4 of Section , T N, R		g <u>-89</u>		l' 52.1			Fe] N] S		Feet W		
Facili		01	1		tate					Village					Feet W		
	-			Randolph	IL		Bald	win	-	_							
Sar	nple								dur		Soil	Prop	erties		_		
	(ii)	ts	set	Soil/Rock Description					PID 10.6 eV Lamp	e (j							
r pe	Att. sred	Joun	In Fe	And Geologic Origin For		s	5	в	.6 e ⁷	essiv h (ts	t e		ity		ents		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Each Major Unit		S C	Graphic Log	Well Diagram	D 10	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	200	RQD/ Comments		
		Bl	De	0 - 0.5' FILL, ASH (Coal): SM, black (10YR 2	2/1)	(FILL)	Grap Log	D A N	Id	Stı Stı	Ž Ů	ĒĒ	Pl ² Inc	Р			
1 CS	120 45		E	$_{\Box}$ silt to sand-sized ash, organic material (5-10											CS= Core Sample		
			-1	_loose, wet. 0.5 - 1.5' FILL, SILTY CLAY: CL/ML, mediur	 m to	(FILL) CL/ML				1							
			Ē	high plasticity, stiff.	_	+	·[/]	8									
			-2	1.5 - 3.2' FILL, ASH (Coal): SM, black (10YF silt to sand-sized ash, wet.	R 2/1),												
			Ē			(FILL) SM											
			-3														
			Ē	3.2 - 4.1' FILL, SILTY CLAY: CL/ML, gray (1 5/1), medium plasticity, soft, moist.	0YR	(FILL)		Ī		0.5							
			-4			ĊL/MĹ				0.5							
			E	4.1 - 11' FILL, ASH (Coal): SM, black (10YR silt to sand-sized ash, wet.	2/1),				-								
			-5														
			-	5.4' very dark gray.													
			-6														
			E														
			-7														
			E			(FILL) SM											
			-8														
			E														
			-9														
			F														
2	48		-10														
2 CS	30		F														
			-11	11 - 11.9' FILL, ASH (Coal): SW-SM, black (10YR												
			-	2/1), silt to sand-sized ash, wet.	lont	(FILL) SW-SM	1										
			-12														
	•	fy that	the inf	formation on this form is true and correct to the		y know	ledge.										
Signa	ture	-	-4	Firm Raml									: (414)				
			/	234 W	Florida	Street,	5th Flo	or, Mil		e, WI 5			: (414)		608		

reet, 5th Floor, Milwaukee, WI 53204 Fax. (414)037-3000 Template: RAMBOLL_IL_BORING LOG - Project: 845_BALDWIN_2022.GPJ

SOIL BORING LOG INFORMATION SUPPLEMENT



			Boring Number XPW01					Pa	ge 2	of	2		
Sample							dui		Soil	Prop	erties		
k (ii	ts	set	Soil/Rock Description				PID 10.6 eV Lamp	e (J					
Number and Type Length Att. & Recovered (in)	Blow Counts	Depth In Feet	And Geologic Origin For	s		я	.6 eV	Compressive Strength (tsf)	e t		ty		ents
Number and Type Length At Recovered	N C	oth I	Each Major Unit	U	Graphic Log	Well Diagram	010	npre	Moisture Content	Liquid Limit	Plasticity Index	00	RQD/ Comments
Nun and Len Rec	Blo	Del		U S	Grap Log	Well Diag1	PIL	Co1 Stre	C ₀₁	Liquid Limit	Plastic Index	P 200	RQD/ Comr
		-	11.9 - 14' SILTY CLAY: CL/ML, dark grayish brown (10YR 4/2), yellowish brown to gray (10YR										
		-13	5/1) mottling (10-20%), medium to high plasticity,					2.75					
			very stiff, moist. <i>(continued)</i>	CL/ML									
								3					
		-14	14' End of Boring.										
	I	I	1	1	I	I		I		I	I	I	

VDW01



F '1'	<u> </u>				T • (D :			T 1		D :		ge 1	of	2
	ty/Proje dwin I				License/	Permit	Monito	oring N	umbe	r	Boring	s Numb XPV			
				of crew chief (first, last) and Firm	Date Dri	lling S	tarted		Da	te Drill	ing Co			Dril	ling Method
	en Lit					0 /2 4	12022								
Cas	scade l	Drilli	ng	Common Well Name	Final Sta		/2022	el	Surfac	e Eleva	9/24/2	2022	Be		Diameter
				XPW02			AVD8			4.86 Fe		AVD			.0 inches
				stimated: 🗌) or Boring Location 🛛			<u>8° 11</u>			Local C					
State		-		5 N, 2,384,171.76 E E/W							_]N		E
Facili	1/4 tv ID	of	1	/4 of Section , T N, R County S	Long		<u>)° 51</u> Civil T			Village	Fe	et L	S		Feet W
1 40111	.y 12				L		Baldy		10), 01	, mug					
Sar	nple								du		Soil	Prop	erties		
	& in)	s	et	Soil/Rock Description					PID 10.6 eV Lamp	e ()					
, e	Att. red (ount	n Fe	And Geologic Origin For					6 eV	ssiv 1 (tsf	e.		y		nts
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Each Major Unit		SCS	Graphic Log	Well Diagram	0 10.	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	200	RQD/ Comments
		Blc	De			n	Grap Log	Well Diag	IId	Str.	Ω̈́Ĕ	Liquic Limit	Plastic Index	P 2	
1 CS	120 120		-	0 - 9.5' FILL, ASH (Coal): SM, greenish black (GLEY 1 2.5/1), silt to sand-sized ash, gravel				Š Š							CS=Core Sample
			-1	(0-5%), loose, moist.											
			E												
			\mathbb{E}_{2}												
			-3												
			-4					·- ·-							
			-			(FILL)									
			-5			SM									
			-6												
			E												
			-7												
			-8												
			-												
			-9												
			-	9.5 - 11' FILL, ASH (Coal): SW-SM, reddish	hlack										
2	48		-10	(2.5YR 2.5/1), silt to sand-sized ash, silt (5-1)	5%),	(FILL)									
2 CS	48		-	moist to wet.		ŚW-SŃ	1								
			-11	11 - 14' SILTY CLAY: CL/ML, dark greenish	arav										
			- -	(GLEY 1 4/1), medium to high plasticity, stiff	to very	CL/ML	E			1.25					
			-12	stiff, moist.			//								
	•	fy that	the inf	ormation on this form is true and correct to the b		y know	ledge.								
Signa	ture	5	-4	Firm Ramb									(414)		
			/	234 W	Florida S	Street, 3	5th Floe	or, Mil RAME	wauke 30LL	e, WI 5	53204 ING LO		(414)		608 DWIN_2022.GPJ

Template: RAMBOLL_IL_BORING LOG - Project: 845_BALDWIN_2022.GPJ

SOIL BORING LOG INFORMATION SUPPLEMENT



Boring Number XPW02	Page 2 of 2
	Soil Properties
Number Number and Type Length Att. & Recovered (iii) Blow Counts Blow Counts Deptih In Feet Number Deptih In Feet US CS US CS US CS US CS Neull Eacy Wall Diagram No PID 10.6 eV Lamp PID 10.6 eV Lamp	Compressive Strength (tsf) Moisture Content Liquid Limit Plasticity Index P 200 P 200 Comments
11 - 14' SILTY CLAY: CL/ML, dark greenish gray (GLEY 1 4/1), medium to high plasticity, stiff to very stiff, moist. (continued) 2 13 13' yellowish brown (10YR 5/4). CL/ML	



Facili	ty/Proje	ot Nor	<u></u>		T	_icense/	Dormit	Monit	oring N	Jumbo	r	Porin	Pa g Numl	ge 1	of	2		
	dwin I			t			I CI IIII	wioniu	Jing I	vuinoc	1	Doring		W04				
Borin	g Drille	d By:	Name	of crew chief (first, last) and Firm	Γ	Date Dri	lling S	tarted		Da	te Drill	ing Co			Dril	ling Method		
	ke We						0/24	10000				0/04/	2022					
Cas	scade l	Drilli	ng	Common Well Name		inal Sta		/2022		Surfa	e Eleva	9/24/	2022	B		Diameter		
				XPW04				AVD8).59 F		AVD			.0 inches		
				stimated: 🗌) or Boring Location 🛛					,		Local				-			
State				1 N, 2,383,618.45 E E/W			t <u>38</u>		<u>' 40.9</u>					N		□ E		
Facili	1/4	of	1	/4 of Section , T N, R County	Sta		<u>g89</u>	$\frac{10^{\circ} - 51}{Civil T}$	<u>' 49.7</u>		Village		eet [S		Feet W		
гасш	ty ID			Randolph	II			Baldy		ny/ oi	vmage	5						
Sar	nple			Tuntooipii				Duiu		d		Soil	Prop	erties	5			
	1 ·		t	Soil/Rock Description						PID 10.6 eV Lamp			<u>r</u>			-		
	ott. & ed (i	unts	Fee	And Geologic Origin For						eV	sive (tsf)					tts		
lber Type	gth A	v Co	th In	Each Major Unit			CS	ohic	ram	10.6	upres ngth	sture	t, id	ticity	0)/ imen		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet				U S I	Graphic Log	Well Diagram	Î E	Compressive Strength (tsf)	Moisture Content	Liquid	Plasticity Index	P 200	RQD/ Comments		
1	120	. –	E	0 - 6' FILL, ASH (Coal): SM, black (10YR :	2/1)	to										CS=Core		
CS	CS 85 very dark gray (10YR 3/1), silt to sand-sized ash, clay (5-15%), gravel (0-5%), wood (0-5%), moist.															Sample		
			1							×								
			E															
			-2															
			E				(=11.1)											
			-3				(FILL) SM											
			E															
			-4															
			-															
			-5															
			F															
			-6	6 - 16.5' FILL, ASH (Coal): SW, black (10)	YR 2	2/1)												
			-	sand-sized ash, silt (10-20%), clay (0-5%),	, loo	se,												
			-7	wet.														
			E															
			-8															
			-9				(FILL) SW											
			F				500											
			-10															
2 CS	60 60		F															
-			-11															
			⊧ îi						l:∃∃:									
			-12															
 I here	by certi	fv that		ormation on this form is true and correct to th	e he	est of m	v know	ledge	1	1	1	1	1	1	1	<u> </u>		
Signa	-	., unat	and mi	Firm Rar		-	, 1110 W	leage.					T_1	: (414	1927 2	607		
0	2	-	-4			511 Florida S	Street, :	5th Flo	or, Mil	lwauke	e, WI 5	53204		: (414				
				=* ;			.7											

 234 W Florida Street, 5th Floor, Milwaukee, WI 53204
 Fax: (414)837-3608

 Template: RAMBOLL_IL_BORING LOG - Project: 845_BALDWIN_2022.GPJ

SOIL BORING LOG INFORMATION SUPPLEMENT



				Boring Number XPW04							Pag	ge 2	of	2
Sar	nple							dune		Soil	Prop	erties		
	Length Att. & Recovered (in)	nts	feet	Soil/Rock Description				PID 10.6 eV Lamp	ive tsf)					6
ype	ch At vered	Cou	l In F	And Geologic Origin For Each Major Unit	S	ji.	am	0.6 6	sressi gth (i	ant	q	city		/ nents
Number and Type	Lengt	Blow Counts	Depth In Feet	Lacit Major Onit	U S C	Graphic Log	Well Diagram	PID 1	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
			-	6 - 16.5' FILL, ASH (Coal): SW, black (10YR 2/1), sand-sized ash, silt (10-20%), clay (0-5%), loose,										
			-13	wet. (continued)										
			_											
			-14		(FILL)									
			-)`sw′									
3 CS	60 50.4		-15	15' interbedded silty clay.										
03	50.4		- 											
			-17	16.5 - 20' SILTY CLAY: CL/ML, greenish gray (GLEY 1 6/1), yellowish brown mottling (10%), sand (0-5%), medium to high plasticity, very stiff, moist.					2.75					
									_					
			-18		CL/ML				3.25					
									3.5					
			-20	20' End of Boring.										
	· 1				'	'			1		1	1		1



Page 1 of 2 Facility/Project Name License/Permit/Monitoring Number Boring Number Baldwin Power Plant XPW05												2				
				t		License/	Permit	Monito	oring N	umber			Numb XPV			
				of crew chief (first, last) and Firm		Date Dri	lling S	tarted		Da	te Drill				Drill	ing Method
	ke We cade l		na				0/2/	/2022				9/24/2	0000		Sc	onic
		71111	ng	Common V	Well Name	Final Sta				Surfac	e Eleva		2022	Bo		Diameter
	~				W05	Fe	et (NA	AVD8	8)		.12 Fe				6	.0 inches
				stimated: \Box) or Boring Locatio 5 N, 2,384,034.20 E E/	n⊠ ®W	La	t <u>38</u>	<u>8° 11</u>	<u>'</u> 46.4	401"	Local C	Jrid Lo				
	1/4			/4 of Section , T N,	-	Lon		<u>° 51</u>				Fe]N]S]	⊢ E Feet □ W
Facili	ty ID			County		State				ity/ or	Village	•				
Sar	nple			Randolph		IL		Baldy	win	d		Soil	Pron	erties		
			L.	Soil/Rock Descrip	otion					PID 10.6 eV Lamp						
o	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	And Geologic Origi					_	5 eV	Compressive Strength (tsf)	0		~		ıts
Number and Type	gth / over	ŭ	oth In	Each Major Un	it		CS	Graphic Log	Well Diagram	10.6	npres	Moisture Content	uid	Plasticity Index	00	RQD/ Comments
Nur and		Blo	Dep				U S	Grap Log	Well Diagr	DId	Cor Stre	Moi Cor	Liquid Limit	Plastic Index	P 200	RQD/ Comm
1 CS	120 55			0 - 21.9' ASH (Coal): (SW)g, black very dark gray (10YR 3/1), sand-	sized ash, s	silt										
			-1	(5-15%), clay (0-5%), organic ma loose, moist.	iterial (0-5%	o),										
			E													
			-2													
			-3													
			F.													
			-4													
			-5													
			-													
			-6				(0)40-									
			Ē				(SW)g									
			-7													
			E													
			-8													
			-													
-9																
			F													
2 CS	120		-10													
CS	88		E													
			-11													
			-12													
I here	by certi	v that		ormation on this form is true and co	rrect to the l	best of m	v know	ledge		1						L
	-						, 110 W						Tel	(414)	837-36	507
	FirmRambollTel:(414)837-3607234 W Florida Street, 5th Floor, Milwaukee, WI 53204Fax:(414)837-3608										e, WI 5					

234 W Florida Street, 5th Floor, Milwaukee, WI 53204 Fax: (414)837-3608 Template: RAMBOLL_IL_BORING LOG - Project: 845_BALDWIN_2022.GPJ

SOIL BORING LOG INFORMATION SUPPLEMENT



				Boring Number XPW05							Pag	ge 2	of	2
Sai	nple							dur		Soil	Prop	erties		
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
3 CS	120 120		-13 -14 -15 -16 -17 -18 -19 -20 -21	0 - 21.9' ASH (Coal) : (SW)g, black (10YR 2/1) to very dark gray (10YR 3/1), sand-sized ash, silt (5-15%), clay (0-5%), organic material (0-5%), loose, moist. <i>(continued)</i> 15' saturated.	(SW)g									
			-22 -23 -24	21.9 - 24.5' ASH (Coal): ML, dark gray (10YR 4/1) to dark grayish brown (10YR 4/2), silt-sized ash, clay (5-15%), sand (0-5%), non-plastic, wet.	ML									
			-25 -26 -27 -28	24.5 - 28.2' ASH (Coal): (SW)g, black (10YR 2/1), sand-sized ash, silt (5-15%), loose, wet.	(SW)g									
			-29	28.2 - 30' SILTY CLAY: CL/ML, gray (10YR 5/1), light yellowish brown (10YR 6/4) mottling, sand (0-5%), very stiff to hard, medium plasticity, moist. 30' End of Boring.	CL/ML				3.5 4.5					
														I



F 11	· /D ·					Page 1 of 2 License/Permit/Monitoring Number Boring Number							2			
	ty/Proje dwin I			ıt		License/	Permit	/Monit	oring I	vumbe	r	Boring	g Numt XPV			
				of crew chief (first, last) and Firm		Date Dri	illing S	tarted		Da	te Drill	ing Co			Dril	ling Method
	en Lit						0/22	/2022				0/ 77 /	1022		C .	- mia
Cas	scade l	Driin	ng	Common	Well Name	Final Sta		/2022 ater Lev		Surfac	e Eleva	9/22/2 tion	2022	Bo		Diameter
				XF	PW06			AVD8			3.06 Fe		AVD			.0 inches
				stimated:) or Boring Location N, 2,382,140.04 E E		Ia	ıt <u>38</u>	8° 11	' 49.0)814"	Local C	Grid Lo				
State	Plane 1/4				E/(W) I, R	Lon			2' 8.2			Fe] N] S		Feet W
Facilit		01		County		State					Village					
	- 1			Randolph		IL		Bald	win							
San	nple									PID 10.6 eV Lamp		Soil	Prop	erties		_
	t. & l (in)	nts	feet	Soil/Rock Descri	-					N L	ive tsf)					~
ber ype	h At /ered	Cou	In F	And Geologic Orig Each Major U	-		s	ii.	am	0.6 6	oress gth (ure	5	city		nent
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet		IIIt		JS C	Graphic Log	Well Diagram	D1	Compressive Strength (tsf)	Moisture Content	Liquid	Plasticity Index	200	RQD/ Comments
1	72	Щ	<u> </u>	0 - 5' FILL, ASH (Coal): SM, bla	ack (10YR 2/	(1) to	D				l S S				Р	CS=Core
ĊS	72		_	very dark grayish brown (10YR sand-sized ash, angular gravel)		y										Sample
			1	(5-15%), loose, moist.	. ,					X						
			Ē													
			E^{-2}				(FILL)									
			È a				SM									
			-3													
			È,													
			-4													
			-5													
			F	5 - 5.4' FILL, ASH (Coal): CL/M ∖gray (GLEY 1 4/1), medium plas	L, dark gree sticitv. soft.	nish ⁄	(FILL) CL/ML		目							
			6	5.4 - 9.9' FILL, ASH (Coal): SM	, black (10YI	R 2/1),			E.							
2 CS	120 120		F	silt to sand-sized ash, clay (5-15	o%), loose, n	noist.										
			-7													
			E	7 - 9.9' interbedded silty clay.			(FILL)		E	•						
			-8				`SM ′		E							
			-9													
			Ē						目							
			-10	9.9 - 16' SILTY CLAY: CL/ML, g	greenish grav	v										
			-	(GLEY 1 6/1), sand (0-5%), orga medium to high plasticity, very s	anic material	Í (0-5%),										
			-11	10.5' light olive brown (2.5Y 5/3 to reddish brown mottling (50%)	3), yellowish	brown	CL/ML	\mathbb{E}								
			-		-											
			-12					 .		•						
	•	fy that	the inf	formation on this form is true and c			y know	ledge.								
Signature E firm Ramboll							II Tel: (414)837-3607 Iorida Street, 5th Floor, Milwaukee, WI 53204 Fax: (414)837-3608									
					254 W	v Florida S	street,	JUL FIO	or, Mi	iwauke	e, wi 5	5204	гах	. (414)	1057-50	000

Template: RAMBOLL_IL_BORING LOG - Project: 845_BALDWIN_2022.GPJ

SOIL BORING LOG INFORMATION SUPPLEMENT



	Boring Number XPW06							Pa	ge 2	of	2
Sample					du		Soil	Prop	erties		
Number and Type Length Att. & Recovered (in) Blow Counts Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
	9.9 - 16' SILTY CLAY: CL/ML, greenish gray (GLEY 1 6/1), sand (0-5%), organic material (0-5%), medium to high plasticity, very stiff, moist. <i>(continued)</i> 13.7' dark greenish gray (GLEY 1 4/1), reddish brown mottling (10%). 16' End of Boring.	CL/ML									

VDW06

Facility/Project Name	Local Grid Location			Well Name
Baldwin Power Plant	ft.	□ N. □ S	ft. \square W.	
		\bigcirc (estimated: \bigcirc) or		
E II' ID		<u>51.1"</u> Long. <u>-89°</u>		
	St. Plane557,53	0 ft. N,	7 ft. E. E/W	
	Section Location of		Г	09/23/2022 E Well Installed By: (Person's Name and Firm)
	1/4 of	1/4 of Sec, T	N, R[
Distance from Waste/ State	Location of Well Re u Upgradient	lative to Waste/Source s □ Sidegradien	GOV. LOUNUM	berAnen Little
Source ft. IL		nt n 🗆 Not Known		Cascade Drilling
A. Protective pipe, top elevation438	<u>3.45</u> ft. (NAV D88)		- 1. Cap and lock	
B. Well casing, top elevation437	7.66 ft. (NAVD88)		 2. Protective cor a. Inside dian 	
C. Land surface elevation435	5.12 ft. (NAVD88)		b. Length:	$\frac{1}{5.0} \text{ ft.}$
D. Surface seal, bottom <u>434.1</u> ft. (NAV			c. Material:	Steel
12. USCS classification of soil near screen:			d. Additional	protection? □ Other □ Ves ⊠ No
$GP \square GM \square GC \square GW \square SW$			If yes, desc	ribe:
$ SM \boxtimes SC \square ML \square MH \square CL $ Bedrock \square	CH 🗆		3. Surface seal:	Bentonite □ Concrete ⊠
13. Sieve analysis attached? □ Yes	s 🖾 No			Other \Box
14. Drilling method used: Rotary			4. Material betw	een well casing and protective pipe:
Hollow Stem Auge				Bentonite
Sonic Other	r 🛛			Other
	_		- 5. Annular space	e seal: a. Granular/Chipped Bentonite
15. Drilling fluid used: Water $\Box 0.2$ Ain				al mud weight Bentonite-sand slurry
Drilling Mud 0 3 None				al mud weight Bentonite slurry
16. Drilling additives used?	s 🖾 No		d% Be	ntonite \ldots Bentonite-cement grout \Box .Ft ³ volume added for any of the above
			f. How insta	-
Describe			i. now mou	Tremie pumped
17. Source of water (attach analysis, if required	d):			Gravity 🖂
			6. Bentonite sea	l: a. Bentonite granules
			b. □1/4 in.	$\boxtimes 3/8$ in. $\square 1/2$ in. Bentonite chips \boxtimes
E. Bentonite seal, top 434.1 ft. (NAV)	D8 <u>8) or 1.0</u> ft.		c	
F. Fine sand, top 431.1 ft. (NAV)	D8 <u>8) or 4.0</u> ft. <	\searrow	a.	terial: Manufacturer, product name & mesh size
				ded ft ³
G. Filter pack, top ft. (NAV)	D8 <u>8) or 5.0</u> ft. <		8. Filter pack m	aterial: Manufacturer, product name & mesh size
100.1	- 0		a	Filtersil
H. Screen joint, top 428.1 ft. (NAV)	D8 <u>8) or 7.0</u> ft. —			ded ft^3
4231 c 01431	Deex 12.0 c		9. Well casing:	Flush threaded PVC schedule $40 \boxtimes$
I. Well bottom 423.1 ft. (NAV)	D8 <u>8) or 12.0</u> ft. <			Flush threaded PVC schedule 80
J. Filter pack, bottom <u>421.1</u> ft. (NAV	D8 <u>8) or 14.0</u> ft. —		- 10. Screen mater	
			a. Screen Ty	e: Factory cut 🛛
K. Borehole, bottom <u>421.1</u> ft. (NAV)	D8 <u>8) or 14.0</u> ft.			Continuous slot
60			h Manafaata	Other
L. Borehole, diameter 6.0 in.			c. Slot size:	
M. O.D. well casing 2.38 in.		\backslash	d. Slotted ler	
		\backslash		rial (below filter pack): None ⊠
N. I.D. well casing 2.07 in.				Other 🗆
I hereby certify that the information on this form		-	dge.	Date Modified: 12/16/2022
Signature	Firm	Ramboll		Tel: (414)837-3607
		234 W Florida Street, 5t	n Floor, Milwauke	e, WI 53204 Fax: (414)837-3608

Facility/Project Name	Local Grid Lo	cation of Well	1			Well Name	
Baldwin Power Plant		$\underline{\qquad}_{\text{ft.}} \underline{\square} \underbrace{N.}_{S.}$	ft.	\Box E. \Box W.			
Facility License, Permit or Monitoring No.		• <u> </u>	imated:) or V			VDW02	
Facility ID	-		4 <u>"</u> Long. <u>-89°</u> _			XPW02 Date Well Installed	
Facility ID			N, <u>2,384,172</u>	ft. E.	Е/		
Type of Well	Section Locat	ion of Waste/S	Source		ΠE	09/24/2022 Well Installed By: (Person's Name	and Firm)
	1/4 of	1/4 of S	Sec, T	_ N, R	🗆 W	Well Installed By: (Person's Name Arlen Little	,
Distance from Waste/ State	u D Upgra	en Relative to	Waste/Source □ Sidegradient	Gov. Lo	ot Number		
Source ft. IL			□ Not Known			Cascade Drilling	
A. Protective pipe, top elevation 43	38.60 ft. (NAV	V D88)		1. Cap ar			🗆 No
B. Well casing, top elevation 43	37.92 ft. (NAV	VD88)			tive cover p le diameter		<u>4.0</u> in.
C. Land surface elevation 43	34.86 ft. (NAV	VD88)		b. Len	-	_	<u>5.0</u> ft.
D. Surface seal, bottom <u>433.9</u> ft. (NA)	VD8 <u>8) of 0</u> f	t.	A STAN	c. Mat	erial:	Steel Other	
12. USCS classification of soil near screen:		<u>Evenykavie</u>			itional prot	ection?	🛛 No
	$\begin{array}{ccc} W \boxtimes & SP \Box \\ L \Box & CH \Box \end{array}$			If ye	es, describe	:	
$ SM \boxtimes SC \square ML \square MH \square Cl $ Bedrock \square				3. Surfac	e seal:	Bentonite Concrete	
13. Sieve analysis attached? \Box Ye	es 🛛 No					Other	
-	ry 🗆			4. Materi	al between	well casing and protective pipe:	
Hollow Stem Aug	2					Bentonite	
Sonic Othe	er 🛛					Other	
			× ×	5. Annula	ar space sea	a. Granular/Chipped Bentonite	\boxtimes
15. Drilling fluid used: Water $\Box 0.2$ A						ud weight Bentonite-sand slurry	
Drilling Mud D 0 3 Nor					-	ud weight Bentonite slurry	
16. Drilling additives used? \Box Ye	es 🛛 No				_% Benton	ite Bentonite-cement grout volume added for any of the above	
					w installed:		
Describe						Tremie pumped	
17. Source of water (attach analysis, if require	ed):					Gravity	\boxtimes
			× × ×	6. Bentor	nite seal:	a. Bentonite granules	
400.0	1.0					$3/8$ in. $\Box 1/2$ in. Bentonite chips	
E. Bentonite seal, top 433.9 ft. (NAV	/D8 <u>8) or 1.0</u>	ft.	88/.			Other 1: Manufacturer, product name & m	
F. Fine sand, top 430.9 ft. (NAV	/D8 <u>8) or 4.0</u>	ft.		a		-	
100.0	5.0	$\langle \rangle$	× ×			ft ³	
G. Filter pack, top <u>429.9</u> ft. (NAV	/D8 <u>8) or 5.0</u>	ft.		-	back materi	al: Manufacturer, product name & n Filtersil	iesh size
H. Screen joint, top <u>428.9</u> ft. (NAV	(D88) or 6.0	ft		a b. Volu	ume added	ft ³	_
11. Sereen jonn, top 11. (1714)	<u>D00701</u>	1.		9. Well c		Flush threaded PVC schedule 40	\boxtimes
I. Well bottom <u>423.9</u> ft. (NAV	/D8 <u>8) or 11.0</u>	ft.			0	Flush threaded PVC schedule 80	
J. Filter pack, bottom <u>422.9</u> ft. (NAV	(D88) or 12.0	ft		O Screen	material:	Other Schedule 40 PVC	
	2011,01				een Type:	Factory cut	\boxtimes
K. Borehole, bottom <u>420.9</u> ft. (NAV	/D8 <u>8) or 14.0</u>	ft.			• •	Continuous slot	
						Other	
L. Borehole, diameter <u>6.0</u> in.							<u>0.010</u> in.
M Ω D well casing 2.38 in			\backslash	c. Slot	t size: tted length:		$\frac{0.010}{5.0}$ in.
M. O.D. well casing 2.38 in.			1			(below filter pack): None	
N. I.D. well casing 2.07 in.						bentonite chips Other	
I hereby certify that the information on this for Signature				e.		Date Modified: 12/16/2022	
Ehr		Name	OOII Florida Street, 5th F	floor Mi	lwaukee W	Tel: (414)837-3607 Tel: (414)837-3608	
		204 VV	i ioniau Succi, Sul I	1001, 1011	wanter, W	100201 ()	

Facility/Project Name	Local Grid Location	n of Well			Well Name	
Baldwin Power Plant	ft.	□ N. □ S	$_ft. \square W.$			
Facility License, Permit or Monitoring No.						
	Lat. 38° 11'	<u>40.9"</u> Long. <u>-89°</u>	<u>51'</u> 49		XPW04	
Facility ID	St. Plane556,50	03 ft. N,2,383,61	8 ft. E	E/W	Date Well Installed	
T (111	Section Location of				10/05/2022	1.5
Type of Well	1/4 of	1/4 of Sec, T	N. R		Well Installed By: (Person's Name a	and Firm)
Distance from Waste/ State	Location of Well Re	elative to waste/Source	Gov. Lot f	Number	Arlen Little	
Source	u 🗆 Upgradient	-			Cascade Drilling	
t. IL		ent n 🗌 Not Known	\sim 1. Cap and 1		Cusedde Dinning ⊠ Yes	
A. Protective pipe, top elevation <u>4</u> 2	<u>34.91</u> ft. (NAV D88)		2. Protective			
B. Well casing, top elevation 42	34.58 ft. (NAVD88)			diameter:		4.0 in.
C. Land surface elevation4.	30.59 ft. (NAVD88)		b. Length	1:	_	<u>5.0</u> ft.
			c. Materi	al:	Steel	\boxtimes
D. Surface seal, bottom <u>429.6</u> ft. (NA	VD88) <u>or</u> ··· ft.		<u> </u>		Other	
12. USCS classification of soil near screen:	2			-	ection?	🛛 No
	W SP D		If yes,	describe:		
$SM \boxtimes SC \square ML \square MH \square C$ Bedrock \square			3. Surface s	seal:	Bentonite	
	es 🖾 No				Concrete	_
					Other	
14. Drilling method used: Rotat Hollow Stem Aug	ry 🗆		4. Material	between	well casing and protective pipe: Bentonite	
	er 🖂				Other	
15. Drilling fluid used: Water $\Box 0.2$ A	ir 🗆			-	a. Granular/Chipped Bentonite	
Drilling Mud					ud weight Bentonite-sand slurry	
			c1 d%		te Bentonite slurry	
16. Drilling additives used? \Box Ye	es 🛛 No				volume added for any of the above	
			f. How		Tremie	
Describe			1. 110w	instanca.	Tremie pumped	
17. Source of water (attach analysis, if require	ed):				Gravity	
			6. Bentonite	e seal·	a. Bentonite granules	
			/		$/8$ in. \Box 1/2 in. Bentonite chips	
E. Bentonite seal, top429.6 ft. (NAV	/D88) or 1.0 ft		/		Other	
					: Manufacturer, product name & me	
F. Fine sand, top 426.1 ft. (NAV	/D8 <u>8) or 4.5</u> ft. \		a		•	
				ne added	ft ³	_
G. Filter pack, top 425.1 ft. (NAV	/D8 <u>8) or 5.5</u> ft. <				l: Manufacturer, product name & m	esh size
	,		a		Filtersil	
H. Screen joint, top <u>424.1</u> ft. (NAV	/D8 <u>8) or 6.5</u> ft. ~			ne added	ft ³	
			9. Well casi	ing:	Flush threaded PVC schedule 40	\boxtimes
I. Well bottom ft. (NAV	/D8 <u>8) or 16.5</u> ft. <				Flush threaded PVC schedule 80	
					Other	
J. Filter pack, bottom ft. (NAV	/D8 <u>8) or 17.5</u> ft. ~		~10. Screen m	naterial: _	Schedule 40 PVC	
			a. Screer	n Type:	Factory cut	\boxtimes
K. Borehole, bottom ft. (NAV	/D8 <u>8) or 20.0</u> ft. <				Continuous slot	
					Other	
L. Borehole, diameter 6.0 in.						0.010
2.20		\backslash	c. Slot si			$\frac{0.010}{10.0}$ in.
M. O.D. well casing 2.38 in.		\backslash	d. Slotte	-		<u>10.0</u> ft.
2.07			11. Backfill i		below filter pack): None pentonite chips Other	
N. I.D. well casing 2.07 in.				5,01	bentonite chips Other	
Thomsher contification to the total of the state		4 40 4b0 bc=4 = f = 1 1			N. N. 10 1 1011 20000	
I hereby certify that the information on this for Signature	rm is true and correc		euge.		Date Modified: 12/16/2022	
E hr	I'''''''	Kambon	4. E1. 3 C1		Tel: (414)837-3607 I 53204 Fax: (414)837-3608	
		234 W Florida Street, 5	th Floor, Milwa	aukee, W	133204 1 4. (+1+)037-3000	

Facility/Project Name	Local Grid Locatio	on of Well			Well Name	
Baldwin Power Plant	ft		$\underline{\qquad} ft. \square W.$			
Facility License, Permit or Monitoring No.						
	-	<u>46.4</u> Long.			XPW05	
Facility ID		063 ft. N,	34,034 ft. E.	E/W	Date Well Installed	
Type of Well	Section Location of				09/24/2022 Well Installed By: (Person's Name a	ad Eima)
Type of well	1/4 of	, T	ſN, R.	\square	-	ind Firm)
Distance from Waste/ State	Location of Well R	celative to waste/Sour	ce Gov. L	Lot Number	Arlen Little	
Source ft. IL	u 🗆 Upgradient	t s □ Sidegra ient n □ Not Kn			Cascade Drilling	
	<u>37.57</u> ft. (NAV D88		$\sim 1.$ Cap a		Yes	
				ctive cover p		
B. Well casing, top elevation 42	37.27 ft. (NAVD88	3) - /		ide diameter		<u>4.0</u> in.
C. Land surface elevation 43	34.12 ft. (NAVD88	3)	b. Le	-		<u>5.0</u> ft.
D. Surface seal, bottom433.1_ ft. (NA)	VD8 <u>8) ol.0</u> ft. 🗸		c. Ma	aterial:	Steel	
				ditional prot	Other Detection?	
12. USCS classification of soil near screen: $GP \square GM \square GC \square GW \square SY$	w⊠ SP □		\ \	-		× NO
	$ \begin{array}{c c} W \boxtimes & SP \Box \\ L \Box & CH \Box \end{array} $			-	Bentonite	-
Bedrock 🗆			∕ [∕] 3. Surfa	ce seal:	Concrete	
13. Sieve analysis attached?	es 🖾 No		\		Other	
14. Drilling method used: Rotar	ry 🗆		4. Mate	rial between	well casing and protective pipe:	
Hollow Stem Aug	er 🗆				Bentonite	
Sonic Othe	er 🛛				Other	
			—— 5. Annu	lar space sea	al: a. Granular/Chipped Bentonite	\boxtimes
6	ir 🗆				nud weight Bentonite-sand slurry	
Drilling Mud D 0 3 Nor					ud weight Bentonite slurry	
16. Drilling additives used? \Box Ye	es 🛛 No			% Benton	iteBentonite-cement groutvolume added for any of the above	
				ow installed	-	
Describe			1. 11	ow instance	Tremie pumped	
17. Source of water (attach analysis, if require	ed):				Gravity	
			6. Bento	onite seal:	a. Bentonite granules	
			/ b. 🗆] 1/4 in. 🛛 🕄	$3/8$ in. $\Box 1/2$ in. Bentonite chips	
E. Bentonite seal, top433.1 ft. (NAV	/D8 <u>8) or 1.0</u> ft.		/		Other	
			7. Fine	sand materia	l: Manufacturer, product name & me	esh size
F. Fine sand, top 418.1 ft. (NAV	/D8 <u>8) or 16.0</u> ft. \	$\backslash \backslash \boxtimes \boxtimes /$	a		2	_
417.1 6 6 6 1	170 c		,		ft ³	1 .
G. Filter pack, top $41/.1$ ft. (NAV	/D8 <u>8) or 17.0</u> ft. \			pack materi	al: Manufacturer, product name & m Filtersil	lesh size
H. Screen joint, top416.1 ft. (NAV	/D8 <u>8) or 18.0</u> ft. ~		a	luma addad	ft ³	_
	100 <u>0/01</u> II.	/	9. Well		Flush threaded PVC schedule 40	\boxtimes
I. Well bottom 406.1 ft. (NAV	/D8 <u>8) or 28.0</u> ft. >		<i>y</i> : wen	cushig.	Flush threaded PVC schedule 80	
Ň	,				Other	
J. Filter pack, bottom ft. (NAV	/D8 <u>8) or 29.0</u> ft. ~		10. Scree	n material:	Schedule 40 PVC	
			a. Sc	reen Type:	Factory cut	\boxtimes
K. Borehole, bottom <u>404.1</u> ft. (NAV	/D8 <u>8) or 30.0</u> ft. \				Continuous slot	
60					Other	
L. Borehole, diameter 6.0 in.				anufacturer ot size:		0.010_ in.
M.O.D. well casing 2.38 in			\ \	ot size: otted length:		10.0 ft.
M. O.D. well casing 2.38 in.			\ \	-	(below filter pack): None	
N. I.D. well casing 2.07 in.					bentonite chips Other	
2						
I hereby certify that the information on this fo			owledge.		Date Modified: 12/16/2022	
Signature	Firm	Kambon			Tel: (414)837-3607	
c		234 W Florida Stree	et, 5th Floor, M	lilwaukee, W	/I 53204 Fax: (414)837-3608	

Facility/Project Name	Local Grid Loc	ation of Well				Well Name	
Baldwin Power Plant		ft. □ N. ft. □ S gin □ (estimat	ft.	□ E. □ W.			
Facility License, Permit or Monitoring No.							
	Lat. <u>38°</u>	11' 49.1"	Long. <u>-89°</u> _	52'		XPW06	
Facility ID		57,324 ft. N,		ft. E.	E/W	Date Well Installed	
Type of Well	1	n of Waste/Sour			ΠE	09/22/2022 Well Installed By: (Person's Name :	and Eima)
Type of well	1/4 of	<u>1/4 of Sec.</u>	, T	_N, R	$\square W$	-	and Firm)
Distance from Waste/ State	Location of we	II Relative to wa	aste/Source	Gov. Lo	ot Number	Arlen Little	
Source ft. IL	u □ Upgrad	radient s \Box	Sidegradient			Cascade Drilling	
	$\frac{18.06}{18.06}$ ft. (NAV)			1. Cap ar		\boxtimes Yes	□ No
					tive cover p		
B. Well casing, top elevation4	17.72 ft. (NAV)	D88)			de diameter		<u>4.0</u> in.
C. Land surface elevation4	18.06 ft. (NAV	D88)		b. Len	-	_	<u>5.0</u> ft.
D. Surface seal, bottom417.1 ft. (NA	VD88) of 0 ft	5.215.21	त्रार्थ	c. Mat	erial:	Steel	
	(<u>)</u> 1000 <u>/</u> 01 11.	1.211.211.2	21, 21, 21		litional prot	ection? Other Yes	
12. USCS classification of soil near screen: $GP \square GM \square GC \square GW \square SY$	W 🗆 SP 🗆				-	: Tes	
	$L \square CH \square$			-		Bentonite	-
Bedrock				3. Surfac	e seal:	Concrete	
13. Sieve analysis attached?	es 🖾 No					Other	
14. Drilling method used: Rotat	ry 🗆			4. Materi	al between	well casing and protective pipe:	
Hollow Stem Aug	jer 🗌					Bentonite	
Sonic Oth	er 🛛				be	ntonite chips Other	\boxtimes
			KXX		-	a. Granular/Chipped Bentonite	
6	ir 🗆					ud weight Bentonite-sand slurry	
Drilling Mud D 0 3 Nor						ud weight Bentonite slurry	
16. Drilling additives used? \Box Ye	es 🖾 No				_% Benton	ite Bentonite-cement grout volume added for any of the above	
			KXX		w installed:	-	
Describe				1. 110	w mstanea.	Tremie pumped	
17. Source of water (attach analysis, if require	ed):					Gravity	
			× e	5. Bentoi	nite seal:	a. Bentonite granules	
				b. 🗆	1/4 in. ⊠3	$3/8$ in. $\Box 1/2$ in. Bentonite chips	\boxtimes
E. Bentonite seal, top ft. (NAV	/D8 <u>8) or 1.0</u> 1	ít. 🚬 👹				Other	
	2.0			7. Fine sa	and materia	l: Manufacturer, product name & me	esh size
F. Fine sand, top 415.1 ft. (NAV	/D8 <u>8) or 3.0</u> f	ît. 🔪 🔪		a		- 2	_
	(Doo) 40					ft ³	
G. Filter pack, top414.1 ft. (NAV	/D8 <u>8) or 4.0</u> f			-	pack materi	 al: Manufacturer, product name & n Filtersil 	lesh size
H. Screen joint, top413.1 ft. (NAV	/D8 <u>8) or 5.0</u>			a b. Volu	habbe amu	ft ³	
	190 <u>0/01</u>		- / .	9. Well c		Flush threaded PVC schedule 40	\bowtie
I. Well bottom 408.1 ft. (NAV	/D8 <u>8) or 10.0</u>	ît. 🥄			81	Flush threaded PVC schedule 80	
						Other	
J. Filter pack, bottom ft. (NAV	/D8 <u>8) or 12.0</u> f	ît	10	0. Screen	material:	Schedule 40 PVC	
				a. Scr	een Type:	Factory cut	
K. Borehole, bottom 402.1 ft. (NAV	/D8 <u>8) or 16.0</u>	ît.				Continuous slot	
60				1 1	6 4	Other	
L. Borehole, diameter 6.0 in.				c. Slo			0.010_ in.
M. O.D. well casing 2.38 in.			\sim		t size: tted length:		$\frac{5.0}{5.0}$ ft.
III.			11		-	(below filter pack): None	
N. I.D. well casing 2.07 in.						bentonite chips Other	
C							
I hereby certify that the information on this fo			of my knowledg	e.		Date Modified: 12/16/2022	
Signature	F	^{irm} Ramboll				Tel: (414)837-3607	
c		234 W Flor	rida Street, 5th F	Floor, Mi	lwaukee, W	/I 53204 Fax: (414)837-3608	

ATTACHMENT 5 PCA Data Summary

ELECTRONIC PCA DATA FOR ATTACHMENT 5 35 I.A.C. § 845: ALTERNATIVE SOURCE DEMONSTRATION BALDWIN POWER PLANT BOTTOM ASH POND COLLINSVILLE, IL

Well	HSU	Date	Well Type	pH (SU)	Alkalinity, total (mg/L)	Barium (mg/L)	Boron (mg/L)	Calcium (mg/L)	Chloride (mg/L)	Fluoride (mg/L)	Lithium (mg/L)	Sulfate (mg
MW-304	BU	03/28/2022	Background	7.78	843	0.0194	1.71	14.5	161	1.76	0.0829	198
MW-304	BU	09/29/2022	Background	7.72	836	0.0183	1.75	10.2	174	1.70	0.0861	199
MW-304	BU	10/26/2022	Background	7.89	825	0.0186	1.76	10.8	175	1.72	0.0869	193
MW-304	BU	11/17/2022	Background	7.87	818	0.0209	1.91	9.48	175	1.7	0.0635	218
MW-304	BU	12/14/2022	Background	7.82	833	0.0191	2.16	10	181	1.82	0.0756	216
MW-304	BU	01/11/2023	Background	7.83	844	0.0173	1.68	8.5	185	1.68	0.0819	209
MW-304	BU	02/20/2023	Background	7.75	854	0.0216	1.75	10.7	186	1.67	0.0818	228
MW-304	BU	03/15/2023	Background	7.77	814	0.0206	1.89	10.6	173	1.67	0.094	208
MW-304	BU	04/04/2023	Background	7.75	853	0.0324	1.69	8.9	168	1.81	0.0808	210
MW-304	BU	05/22/2023	Background	7.51	836	0.0199	1.7	9.63	162	1.72	0.0603	208
MW-304	BU	08/03/2023	Background	7.92	838	0.0201	1.6	11.4	160	1.70	0.0779	188
MW-304	BU	11/01/2023	Background	7.81	855	0.0199	1.7	12	166	1.91	0.0807	191
MW-304	BU	02/05/2024	Background	7.70	818	0.0295	1.5	12.4	155	1.77	0.0763	185
MW-304	BU	04/16/2024	Background	7.81	805	0.0199	1.7	13.0	161	1.69	0.0823	195
MW-358	BU	10/27/2022	Background	7.93	633	0.0933	1.1	12.8	688	2.43	0.0621	108
MW-358	BU	11/17/2022	Background	7.83	758	0.1720	1.25	15.8	992	2.36	0.0592	101
MW-358	BU	12/13/2022	Background	8.45	859	0.168	1.67	19	1120	2.1	0.0696	71
MW-358	BU	01/11/2023	Background	7.59	841	0.165	1.38	14.0	1200	2.73	0.0957	34
MW-358	BU	02/20/2023	Background	8.38	847	0.201	1.42	13.2	1330	2.87	0.102	16
MW-358	BU	03/13/2023	Background	7.73	856	0.166	1.51	10.9	1340	3.07	0.115	8
MW-358	BU	04/04/2023	Background	7.71	851	0.261	1.45	11.4	1370	3.13	0.105	31
MW-358	BU	05/19/2023	Background	7.62	835	0.192	1.6	12.5	1300	3.31	0.0778	10
MW-358	BU	03/19/2023	Background	8.00	843	0.192	1.6	9.9	1300	3.31	0.0778	9
MW-358 MW-358	BU	11/01/2023	-	7.89	840	0.235	1.38	11.3	1290	3.36	0.0981	11
	BU	02/06/2024	Background	7.89	712	0.162		30.3	917		-	20
MW-358		02/06/2024	Background	7.91	532		0.771	30.3		2.4	0.115	19
MW-358	BU	03/29/2022	Background	7.69	391	0.12	0.277		458	1.53	0.0425	_
MW-370	BU		Downgradient				1.6	34.2	1470	3.15	0.223	270
MW-370	BU	09/30/2022	Downgradient	7.64	403	0.0589	2.67	51.4	1520	2.98	0.21	273
MW-370	BU	10/27/2022	Downgradient	6.88	389	0.0380	1.84	39.6	1320	3.11	0.137	250
MW-370	BU	11/17/2022	Downgradient	7.79	388	0.0292	1.74	36.8	1450	3.06	0.110	278
MW-370	BU	12/14/2022	Downgradient	7.52	394	0.0325	2.34	44.7	1430	3.12	0.118	263
MW-370	BU	01/12/2023	Downgradient	7.50	393	0.0272	1.75	38.4	1470	3.07	0.133	253
MW-370	BU	02/21/2023	Downgradient	7.46	389	0.0303	1.95	40.6	1570	2.86	0.146	273
MW-370	BU	03/14/2023	Downgradient	7.45	402	0.029	1.9	40	1340	2.96	0.160	251
MW-370	BU	04/03/2023	Downgradient	7.53	386	0.0308	2.1	37.4	1280	3.16	0.158	253
MW-370	BU	05/16/2023	Downgradient	7.47	399	0.0321	1.85	37.0	1360	3.07	0.12	253
MW-370	BU	08/03/2023	Downgradient	7.79	399	0.033	1.73	41.4	1310	3.06	0.134	243
MW-370	BU	11/02/2023	Downgradient	7.61	413	0.0285	2.0	41.1	1420	3.7	0.124	273
MW-370	BU	02/06/2024	Downgradient	7.39	410	0.0417	1.69	40.1	1460	3.28	0.169	257
MW-370	BU	04/16/2024	Downgradient	7.59	393	0.042	1.76	39.5	1460	3.33	0.17	247
MW-392	BU	10/27/2022	Downgradient	6.98	446	0.029	1.57	22.1	334	3.19	0.0474	149
MW-392	BU	11/16/2022	Downgradient	7.98	388	0.046	1.72	27.2	648	3.36	0.0512	83
MW-392	BU	12/13/2022	Downgradient	7.70	381	0.0462	2.33	30	918	3.98	0.0646	50
MW-392	BU	01/12/2023	Downgradient	7.63	413	0.042	1.66	47.1	888	3.96	0.076	47
MW-392	BU	02/20/2023	Downgradient	7.60	370	0.0399	1.97	30.4	909	3.69	0.0799	68
MW-392	BU	03/13/2023	Downgradient	7.67	381	0.0397	1.92	28.1	896	4.01	0.0767	57
MW-392	BU	04/03/2023	Downgradient	7.73	379	0.057	2.7	30.5	834	4.18	0.117	61
MW-392	BU	05/16/2023	Downgradient	7.54	372	0.0414	1.92	25.6	827	4.07	0.0675	63
MW-392	BU	08/03/2023	Downgradient	7.86	359	0.0407	1.82	26.0	878	4.07	0.0733	55
MW-392	BU	10/31/2023	Downgradient	7.65	384	0.0615	1.91	50.8	871	4.52	0.0733	66
MW-392	BU	02/06/2024	Downgradient	7.64	378	0.0551	1.71	25.3	863	4.32	0.108	59
	BU	04/16/2024		7.67	370	0.0521	1.74	25.0	868	4.42	0.0746	42
MW-392		10/27/2022	Downgradient	7.67				9				
MW-393	BU		Downgradient		641 672	0.02	1.83		436	5.86	0.0767	285
MW-393	BU	11/16/2022	Downgradient	8.11		0.03	1.53	11	475	5.95	0.0722	280
MW-393	BU	12/14/2022	Downgradient	8.64	666	0.0246	2.04	11	445	5.79	0.0603	263
MW-393	BU	01/12/2023	Downgradient	7.89	812	0.0288	1.61	14.7	633	8.02	0.0807	232
MW-393	BU	02/20/2023	Downgradient	7.95	822	0.0304	1.74	11	640	7.66	0.0853	214
MW-393	BU	03/13/2023	Downgradient	8.03	859	0.0273	1.79	7.9	606	8.21	0.0668	186
MW-393	BU	04/03/2023	Downgradient	8.12	833	0.0481	2.76	8.6	648	9.27	0.123	209
MW-393	BU	05/15/2023	Downgradient	8.28	914	0.0261	1.72	8.4	745	8.42	0.0442	123
MW-393	BU	08/03/2023	Downgradient	8.36	862	0.0269	1.66	6.0	610	7.32	0.0593	134
MW-393	BU	10/31/2023	Downgradient	8.19	827	0.0582	1.59	7.9	723	9.63	0.0672	184
WW-393	BU	02/06/2024	Downgradient	8.12	831	0.06	1.63	6.4	741	9.27	0.1100	206
MW-393	BU	04/16/2024	Downgradient	8.16	816	0.04	1.83	7.1	779	9.22	0.0714	217
TPZ-164	CCR	03/29/2022	CCR	7.31	198	0.11	1.56	55.4	50	0.26	0.0167	227
TPZ-164	CCR	09/30/2022	CCR	7.14	206	0.17	2.04	68.5	52	0.24	0.0243	150
TPZ-164	CCR	10/28/2022	CCR	7.31	276	0.06	1.47	67.6	57	0.26	0.0140	127
FPZ-164	CCR	11/16/2022	CCR	7.56	250	0.06	1.38	61.8	46	0.26	0.0085	123
TPZ-164	CCR	12/14/2022	CCR	7.34	233	0.05	1.54	60.9	55	0.27	0.0114	120
TPZ-164	CCR	03/14/2023	CCR	7.21	283	0.06	1.30	70	43	0.22	0.0101	113
TPZ-164	CCR	08/07/2023	CCR	7.38	293	0.07	1.23	70	51	0.31	0.0151	109
FPZ-164	CCR	02/28/2024	CCR	7.13	285	0.07	0.92	75	52	0.25	0.0099	130
TPZ-164	CCR	04/18/2024	CCR	7.25	275	0.07	1.05	77	49	0.29	0.0115	118
XPW-01	CCR	10/26/2022	CCR	7.03	203	0.10	0.93	65.4	21	0.61	0.0142	98
XPW-01	CCR	11/15/2022	CCR	6.98	205	0.11	1.03	72.5	22	0.50	0.0127	105
XPW-01	CCR	12/13/2022	CCR	6.57	204	0.27	0.94	81.5	25	0.50	0.0354	120
XPW-01	CCR	01/12/2023	CCR	6.86	212	0.11	0.88	67.5	26	0.51	0.0132	119
XPW-01	CCR	05/23/2023	CCR	7	163	0.0743	0.649	55.1	21	0.62	0.0083	62
XPW-01	CCR	08/03/2023	CCR	6.75	218	0.103	0.893	71.5	28	0.58	0.0117	82
XPW-01	CCR	02/08/2024	CCR	6.6	217	0.116	0.961	84.8	49	0.53	0.0117	126
XPW-01 XPW-01	CCR	04/18/2024	CCR	6.88	204	0.0952	0.563	70.2	45	0.55	0.0110	120
XPW-01 XPW-02	CCR	10/26/2022	CCR	7.57	427	0.205	1.18	121	33	0.61	0.0233	22
XPW-02 XPW-02	CCR	11/15/2022	CCR	7.6	426	0.194	1.13	115	30	0.55	0.0233	20
XPW-02 XPW-02		12/12/2022		7.53	374	0.194	1.2	115	30	0.55	0.0194	37
	CCR		CCR	7.53	374		0.87		29			43
XPW-02 XPW-02	CCR	01/12/2023 05/23/2023	CCR		337	0.125		88.5		0.46	0.0108	43
	CCR	10/28/2023	CCR	7.05	222	0.185	1.08	101	36	0.5		-
XPW-04	CCR		CCR	8.31		0.161	1.28	47.9	55	0.44	0.0108	119
XPW-04	CCR	11/15/2022	CCR	8.4	226	0.171	1.15	53.2	56	0.4	0.0066	124
XPW-04	CCR	12/12/2022	CCR	8.04	217	0.196	1.38	51.1	55	0.42	0.0136	120

XPW-04	CCR	12/12/2022	CCR	8.04	217	0.196	1.38	51.1	55	0.42	0.0136	120
XPW-04	CCR	01/12/2023	CCR	7.96	226	0.156	0.835	49.6	54	0.4	0.009	119
XPW-04	CCR	05/23/2023	CCR	8.23	200	0.172	0.921	56.2	45	0.33	0.0056	173
XPW-05	CCR	10/26/2022	CCR	7.82	180	0.104	1.02	43.9	46	0.57	0.0053	123
XPW-05	CCR	11/15/2022	CCR	7.67	180	0.12	1.16	43.5	46	0.58	0.0039	132
XPW-05	CCR	12/12/2022	CCR	7.18	212	0.19	1.25	43.6	48	0.62	0.0093	137
XPW-05	CCR	01/24/2023	CCR	7.3	192	0.208	1.57	40.2	48	0.6	0.008	125
XPW-05	CCR	05/23/2023	CCR	7.16	218	0.212	1.08	45.8	47	0.54	0.0027	110
XPW-05	CCR	08/03/2023	CCR	7.17	229	0.223	0.928	49.1	46	0.55	0.0054	89
XPW-05	CCR	02/28/2024	CCR	7.19	238	0.284	0.977	56.2	47	0.53	0.0093	123
XPW-05	CCR	04/18/2024	CCR	7.03	267	0.294	0.87	60.4	51	0.49	0.0061	114
XPW-06	CCR	10/26/2022	CCR	7.22	370	0.274	2.29	130	25	0.58	0.0118	575
XPW-06	CCR	11/15/2022	CCR	7.27	372	0.198	4.64	164	18	0.61	0.0019	475
XPW-06	CCR	12/13/2022	CCR	7.04	371	0.246	3.86	174	18	0.59	0.0075	508
XPW-06	CCR	01/12/2023	CCR	7.25	278	0.1	3.38	112	10	0.5	0.0031	391
XPW-06	CCR	05/23/2023	CCR	7.23	247	0.161	2.11	75.9	6	0.32	0.0019	171
XPW-06	CCR	08/03/2023	CCR	6.96	195	0.142	1.55	61.6	2	0.37	0.006	117
XPW-06	CCR	02/06/2024	CCR	7.28	244	0.201	2.91	90.6	5	0.35	0.0057	315
XPW-06	CCR	04/18/2024	CCR	7.16	256	0.129	2.64	69.3	2	0.39	0.0058	103

Notes:

Notes: mg/L = milligrams per liter TDS= Total Dissolved Solids SU= standard units HSU = hydrostratigraphic unit CCR = coal combustion residual BU = Bedrock Unit

ATTACHMENT 6

Lithium Isotope Ratio Laboratory Analytical Report



Analytical Results

SiREM File Reference: S-9990

Client: Geosyntec Consultants, Inc. Client Project Number: GLP8063 Date Samples Received: August 24, 2023 Date Samples Analyzed: August/September 2023 IsoDetect Internal Project No: 23-71-GG

Client Sample ID	SiREM Reference ID	Isodetect Reference ID	Client Sample Date	δ ⁷ Li	2SD	Lithium Concentration
		Reference iD	Sample Date	[‰]	[‰]	ug/L
Cooling Pond - 20230821	23-14918	23-71-GG-01	21-Aug-23	35.18	0.74	3.1
MW158R - 20230822	23-14919	23-71-GG-02	22-Aug-23	31.47	0.54	22.6
PZ170-20230821	23-14920	23-71-GG-03	21-Aug-23	16.95	0.73	44.0
TPZ164-20230821	23-14921	23-71-GG-04	21-Aug-23	17.07	0.75	27.6
MW370-20230821	23-14922	23-71-GG-05	21-Aug-23	20.65	0.73	227.0
MW358-20230822	23-14923	23-71-GG-06	22-Aug-23	26.04	0.70	185.0

Comments:

Method: Compound Specific Isotope Analysis (CSIA) -- = not applicable 2SD= standard deviation, calculated from two independent consecutive measurements ug/L = micrograms per liter n.m. = not measured

Analyst:

Brooke Rapien

Brooke Rapien Laboratory Technician II

Results approved:

Date:

Brent G. Paulter **Chemistry Services Manager**

October 10, 2023



06th of October 2023

Analytical report

Ordering party:	SIREM
	130 Stone Rd. West
	Guelph, Ontario,
	Canada N1G 3Z2

Contact person: Ximena Druar Brent G. Pautler, Ph.D.

Contractor:

Isodetect GmbH Deutscher Platz 5b 04103 Leipzig Germany

Person in charge: Kevin Kuntze, Ph.D. Phone: +49 341 35535851 Mail: kuntze@isodetect.de

> Anko Fischer, Ph.D. Phone: +49 341 35535855 Mail: fischer@isodetect.de

11.09.2023

Samples received:

Project ID/ Field site: S-9990

23-71-GG **Internal Project No.:**

Scope on analysis: 6 x isotope ratio of Li

Dr. Kevin Kuntze

to Esdas

Dr. Anko Fischer



Analysis results

Well/sample	Lab ID	δ ⁷ Li [‰]	2SD [‰]	Li [µg/l]
Cooling Pond - 20230821	23-71-GG-01	35.18	0.74	3.1
MW158R-20230821	23-71-GG-02	31.47	0.54	22.6
PZ170-20230821	23-71-GG-03	16.95	0.73	44.0
TPT164-20230821	23-71-GG-04	17.07	0.75	27.6
MW370-20230821	23-71-GG-05	20.65	0.73	227.0
MW358-20230821	23-71-GG-06	26.04	0.70	185.0

The analyses were carried out by MC-ICP-MS using an internal standardization and external calibration with bracketing isotope standard reference materials (SRMs), for which Li delta value (δ^7 Li) was calculated against LSVEC NIST 8545 RM. The standard deviation (2SD) was calculated from two independent consecutive measurements.

Chain of Custody for CSIA of organic pollutants



Isodetect Umweltmonitoring GmbH

Sector Sector	Contact information				Project information						
company:	SiREM		Email:	xdruar@s	siremlab.com	Project ID:	Baldwin GW C				
ontact:	Ximena Druar			130 Stone	e Road W,	Project descrip					
hone:	519-880-5424		Address:		NN N1G 3Z2 Canada	Sampled by:			Company:	Geosy	intec
Clie	ent Sample ID/	Sam	pling	Matrix	Conditions	Sampling	Sample volume	S. C. S.	CSIA	Isotope	Other Notes
Sa	impling point	Date	Time	Watrix	(e.g. Temp., O2, Rh, pH)	type ⁹	for CSIA	Fixative"	for*	ratio^	(e.g. troubles, weather
	Pond - 20230821	8/21/2023	13:20	Water		2	2x500mL VV		Total & Stat	le Li Isoto	
MW158F	R-20230822	8/22/2023	13:50	Water		2	2x500mL VV		Total & Sta		
PZ170-2	20230821	8/21/2023	11:25	Water		2	2x500mL V V		Total & Sta		
	-20230821	8/21/2023	10:45	Water		2	2x500mL V V		Total & Sta	the second s	
MW370-	-20230821	8/21/2023	12:10	Water		21 5	2x500mL V		Total & Sta		the second se
MW358-	20230822	8/22/2023	12:15	Water		2	2x500mL V V		Total & Sta		and the second se
E.											
1 – Submers	ible pump, 2 – Suction pu	mp, 3 – Baile	er, 4 – Tap/c	outlet. 5 – Trial	pit, 6 – Percussion drilling, 7 – I	Direct nush sampli	ng 8 - Hand avcauati	on Q others (alua sa a dina t		
1 – BTEX, 2 - – Petroleum	 halogenated VOC, 3 – P hydrocarbons (e.g. alkyla 	AH, 4 – Fuel a ated benzene	additives (M es, alkanes e	ITBE, ETBE, TA etc.), 7 – Chloro	ME, TAEE etc.), 5 – Explosives (1 obenzenes, 8 – Gas hydrocarbor (give target compounds)	INT. RDX. dinitrot	oluene nitrohenzenes	etc.)	and sampling t	(he)	
	2 - ² H/ ¹ H, 3 - ³⁷ Cl/ ³⁵ Cl, 4			and the second se	the second se						
	- Na ₃ PO ₄ ·12H ₂ O, 3 - HCI										

Relinquished by	Received by	Relinquished by	Received by	
enature Ausan Moman	Signature: 1 Mm Mm	Signature:	Signature:	
Susan Thomas	Name: Vazquez Ramos 1028	Name:	Name:	
ampany: SiREM	Company: 150 defect GmbH	Company:	Company:	
ate/Time: 9-6-2023	Date/Time: 11.09.2023	Date/Time:	Date/Time:	

Isodetect GmbH, Deutscher Platz 5b, 04103 Leipzig, Germany

Phone: +49 (0)341-355-35851, Fax: +49 (0)341-355-35852, Email: kuntze@isodetect.de www.isodetect.de

ATTACHMENT 7

Solid Phase Anions Laboratory Analytical Report



SGS Canada Inc. P.O. Box 4300 - 185 Concession St. Lakefield - Ontario - KOL 2HO Phone: 705-652-2000 FAX: 705-652-6365

Ramboll Americas Engineering Solutions, Inc.

Attn : Evvan Plank

P.O# Box 4873 Syrascuse, New York 13221-7873, USA

Phone: 315-463-7554 Fax:

28-February-2023

Date Rec. :	24 November 2022
LR Report:	CA19226-NOV22
Reference:	Baldwin Power Plant Drilling

Copy: #1

CERTIFICATE OF ANALYSIS Final Report

Analysis	1: Analysis Start Anal Date		3: Analysis mpleted DateCon	4: Analysis npleted Time	6: MW-358 (47-49)	7: MW-358 (86-88)	8: MW-392 (80-82)	12: MW-392 (66-68)
Sample Date & Time					06-Oct-22 15:00	08-Oct-22 18:00	26-Sep-22 16:00	26-Sep-22 12:00
CI [µg/g]	15-Dec-22	20:55			22	70	34	45
SO4 [µg/g]	15-Dec-22	20:55	29-Dec-22	13:45	50	620	280	100
F [%]	08-Dec-22	18:18	12-Dec-22	08:47	0.091	0.091	0.42	0.095
TKN [as N %]	30-Nov-22	09:28	02-Dec-22	11:00	0.06	0.05	< 0.01	0.05
Ra226 [Bq/g]	12-Dec-22	08:48	12-Dec-22	14:33	0.07	< 0.01	0.09	< 0.01

ATHARINE ARNOL Catharine Aunold CHEMIST

Catharine Arnold, B.Sc., C.Chem Project Specialist, Environment, Health & Safety

0003246129

Results relate only to the sample tested. Data reported represents the sample submitted to SGS. Reproduction of this analytical report in full or in part is prohibited without prior written approval. Please refer to SGS General Conditions of Services located at https://www.sgs.ca/en/terms-and-conditions (Printed copies are available upon request.) Test method information available upon request. "Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples. SGS Canada Inc. Environment-Health & Safety statement of conformity decision rule does not consider uncertainty when analytical results are compared to a specified standard or regulation.



SGS Canada Inc. P.O. Box 4300 - 185 Concession St. Lakefield - Ontario - KOL 2HO Phone: 705-652-2000 FAX: 705-652-6365

LR Report : CA19226-NOV22

OnLine LIMS

Page 2 of 2

Fage 2 of 2
 Fage 2 of 2
 Results relate only to the sample tested. Data reported represents the sample submitted to SGS. Reproduction of this analytical report in full or in part is prohibited without prior written approval. Please refer to SGS General Conditions of Services located at https://www.sgs.ca/en/terms-and-conditions (Printed copies are available upon request.)
 Test method information available upon request. "Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.
 SGS Canada Inc. Environment-Health & Safety statement of conformity decision rule does not consider uncertainty when analytical results are compared to a specified standard or regulation.

ATTACHMENT 8

X-ray Diffraction Laboratory Analytical Report



Quantitative X-Ray Diffraction by Rietveld Refinement

Report Prepared for:	Environmental Services
Project Number/ LIMS No.	Custom XRD/MI4508-DEC22
Sample Receipt:	December 7, 2022
Sample Analysis:	December 15, 2022
Reporting Date:	April 24, 2023
Instrument:	BRUKER AXS D8 Advance Diffractometer
Test Conditions (Bulk):	Co radiation, 35 kV, 40 mA; Detector: LYNXEYE Regular Scanning: Step: 0.02°, Step time: 0.75s, 20 range: 6-80°
Test Conditions (Clay):	Co radiation, 35 kV, 40 mA; Detector: LYNXEYE Regular Scanning: Step: 0.02°, Step time: 1s, 2θ range: 3-80° Clay Section Scanning: Step: 0.01°, Step time:0.2s, 2θ range: 3-40°
Interpretations:	PDF2/PDF4 powder diffraction databases issued by the International Center for Diffraction Data (ICDD). DiffracPlus Eva and Topas software.
Detection Limit:	0.5-2%. Strongly dependent on crystallinity.
Contonto	1) Method Summany

Contents:

Method Summary
 Quantitative XRD Results
 XRD Pattern(s)

Kim Gibbs, H.B.Sc., P.Geo. Senior Mineralogist

Haym they

Huyun Zhou, Ph.D., P.Geo. Senior Mineralogist

ACCREDITATION: SGS Natural Resources Lakefield is accredited to the requirements of ISO/IEC 17025 for specific tests as listed on our scope of accreditation, including geochemical, mineralogical and trade mineral tests. To view a list of the accredited methods, please visit the following website and search SGS Canada Inc. - Minerals: https://www.scc.ca/en/search/palcan.

SGS Natural Resources P.O. Box 4300, 185 Concession Street, Lakefield, Ontario, Canada K0L 2H0 a division of SGS Canada Inc. Tel: (705) 652-2000 Fax: (705) 652-6365 www.sgs.com www.sgs.com/met Member of the SGS Group (SGS SA)



Method Summary

The Rietveld Method of Mineral Identification by XRD (ME-LR-MIN-MET-MN-D05) method used by SGS Natural Resources is accredited to the requirements of ISO/IEC 17025.

Mineral Identification and Interpretation.

Mineral identification and interpretation involves matching the diffraction pattern of an unknown material to patterns of single-phase reference materials. The reference patterns are compiled by the Joint Committee on Powder Diffraction Standards - International Center for Diffraction Data (JCPDS-ICDD) database and released on software as Powder Diffraction Files (PDF).

Interpretations do not reflect the presence of non-crystalline and/or amorphous compounds, except when internal standards have been added by request. Mineral proportions may be strongly influenced by crystallinity, crystal structure and preferred orientations. Mineral or compound identification and guantitative analysis results should be accompanied by supporting chemical assay data or other additional tests.

Clay Mineral Separation and Identification:

Clay minerals are typically fine-grained (<2 µm) phyllosilicates in sedimentary rock. Due to the poor crystallinity and fine size of clay minerals, separation of the clay fraction from bulk samples by centrifuge is required. A slide of the oriented clay fraction is prepared and scanned followed by a series of procedures (the addition of ethylene glycol and high temperature heating). Clay minerals are identified by their individual diffraction patterns and changes in their diffraction pattern after different treatments. Clay speciation and mineral identification of the bulk sample are performed using DIFFRACplus EVA (Bruker AXS).

Quantitative Rietveld Analysis:

Quantitative Rietveld Analysis is performed by using Topas 4.2 (Bruker AXS), a graphics based profile analysis program built around a non-linear least squares fitting system, to determine the amount of different phases present in a multicomponent sample. Whole pattern analyses are predicated by the fact that the X-ray diffraction pattern is a total sum of both instrumental and specimen factors. Unlike other peak intensity-based methods, the Rietveld method uses a least squares approach to refine a theoretical line profile until it matches the obtained experimental patterns.

Rietveld refinement is completed with a set of minerals specifically identified for the sample. Zero values indicate that the mineral was included in the refinement calculations, but the calculated concentration was less than 0.05wt%. Minerals not identified by the analyst are not included in refinement calculations for specific samples and are indicated with a dash.

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WARNING: The sample(s) to which the findings recorded herein (the "Findings") relate was(were) drawn and / or provided by the Client or by a third party acting at the Client's direction. The Findings constitute no warranty of the sample's representativeness of any goods and strictly relate to the sample(s). The Company accepts no liability with regard to the origin or source from which the sample(s) is/are said to be extracted.

- - - -



	MW-358 (13-15)	MW-358 (47-49)	MW-358 (86-88)	MW-392 (80-82)	MW-392 (32-33.5)	MW-393 (24-25.5)	MW-394 (20.5-22)	MW-392 (66-68)
Mineral/Compound	DEC4508-1	DEC4508-2	DEC4508-3	DEC4508-4	DEC4508-5	DEC4508-6	DEC4508-7	DEC4508-8
	(wt %)	(wt %)	(wt %)	(wt %)				
Quartz	52.7	29.2	30.7	29.8	52.1	64.1	55.4	22.7
Muscovite	7.7	18.8	19.7	13.1	9.0	5.5	7.6	15.9
Albite	12.3	0.4	2.5	0.6	9.1	6.4	12.8	0.6
Microcline	7.3	8.6	5.9	1.0	6.5	10.1	7.3	5.1
Diaspore	0.3	-	-	-	-	0.2	0.5	2.8
Magnetite	0.9	0.5	0.3	1.4	0.1	0.0	0.1	0.1
Anatase	0.2	0.8	1.8	0.8	0.6	0.3	0.3	1.0
Calcite	-	0.5	1.0	28.1	0.0	0.0	0.2	14.9
Fluorapatite	-	-	-	2.7	0.3	-	0.2	0.2
Ankerite	-	-	-	-	1.4	0.9	0.5	0.8
Clay								
Kaolinite	5.3	4.8	15.0	5.5	6.8	3.2	4.2	3.6
Montmorillonite-12A	4.9	6.8	4.8	-	-	-	-	5.8
Montmorillonite-14A	-	-	-	3.5	3.3	3.5	3.6	-
Nontronite	0.6	4.6	4.3	4.2	1.6	1.4	0.5	3.3
Illite/Mont - 11A	-	8.8	2.7	3.6	2.7	2.1	3.0	7.1
Illite	5.0	15.0	9.2	4.1	0.7	1.0	0.6	10.4
Chlorite IIb	2.6	1.3	2.0	1.6	5.8	1.2	3.1	6.1
TOTAL	100	100	100	100	100	100	100	100

Summary of Rietveld Quantitative Analysis X-Ray Diffraction Results

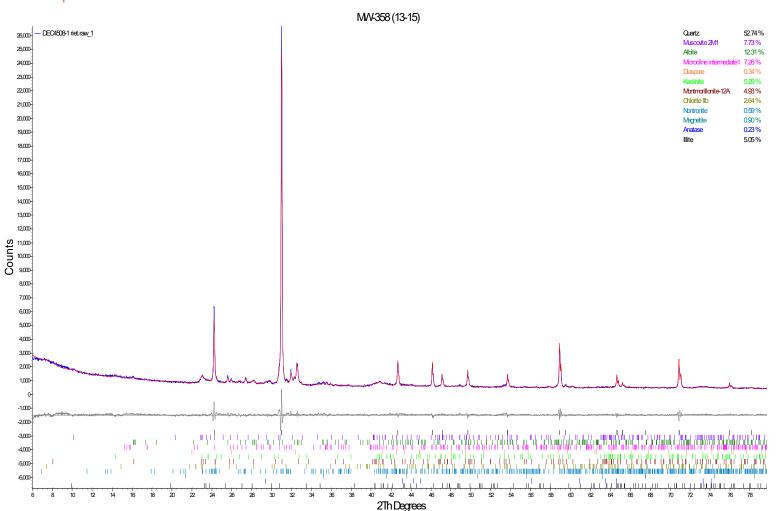
Zero values indicate that the mineral was included in the refinement, but the calculated concentration is below a measurable value.

Dashes indicate that the mineral was not identified by the analyst and not included in the refinement calculation for the sample.

The weight percent quantities indicated have been normalized to a sum of 100%. The quantity of amorphous material has not been determined.

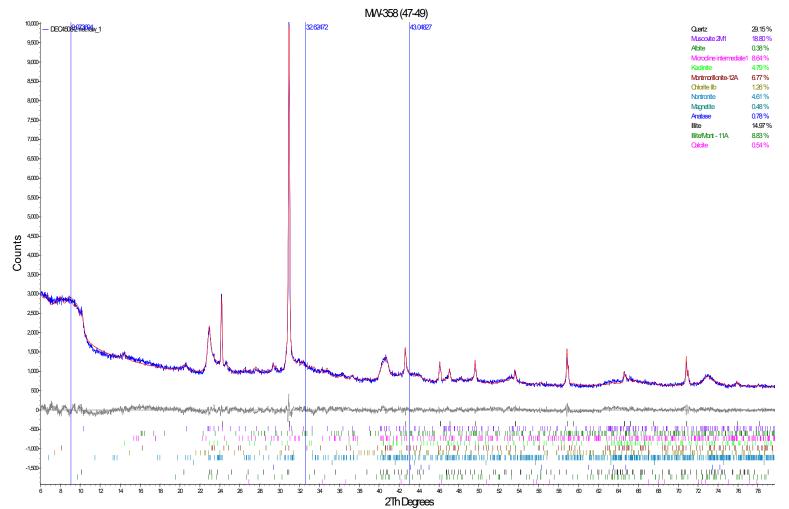
Mineral/Compound	Formula				
Quartz	SiO ₂				
Muscovite	KAI ₂ (AISi ₃ O ₁₀)(OH) ₂				
Albite	NaAlSi ₃ O ₈				
Microcline	KAISi ₃ O ₈				
Diaspore	aAlO.OH				
Magnetite	Fe ₃ O ₄				
Anatase	TiO ₂				
Calcite	CaCO ₃				
Fluorapatite	Ca ₅ (PO ₄) ₃ F				
Ankerite	CaFe(CO ₃) ₂				
Kaolinite	Al ₂ Si ₂ O ₅ (OH) ₄				
Montmorillonite	(Na,Ca) _{0.3} (Al,Mg) ₂ Si ₄ O ₁₀ (OH) ₂ ·10H ₂ O				
Nontronite	Fe ₂ (Al,Si) ₄ O ₁₀ (OH) ₂ Na _{0.3} (H ₂ O) ₄				
Illite/Mont	KAI ₄ (Si,AI) ₈ O ₁₀ (OH) ₄ ·4H ₂ O				
Illite	(K,H ₃ O)(Al,Mg,Fe) ₂ (Si,Al) ₄ O ₁₀ [(OH) ₂ ,(H ₂ O)]				
Chlorite	(Fe,(Mg,Mn) ₅ ,Al)(Si ₃ Al)O ₁₀ (OH) ₈				





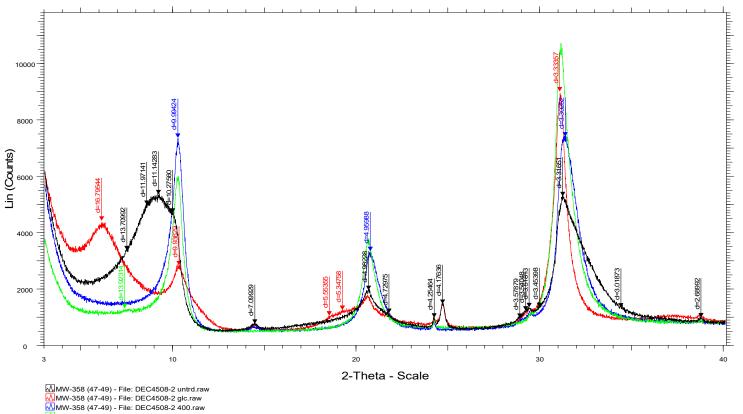
SGS Natural Resources, P.O. Box 4300, 185 Concession Street, Lakefield, Ontario, Canada KOL 2H0





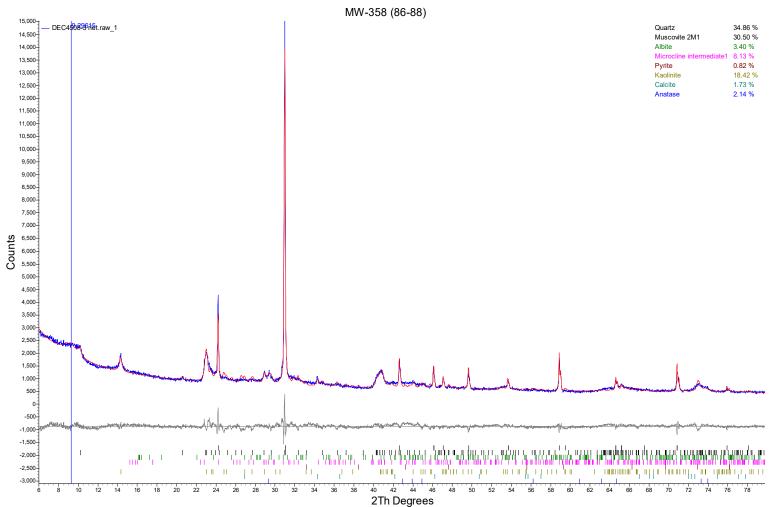


MW-358 (47-49)



MW-358 (47-49) - File: DEC4508-2 550.raw

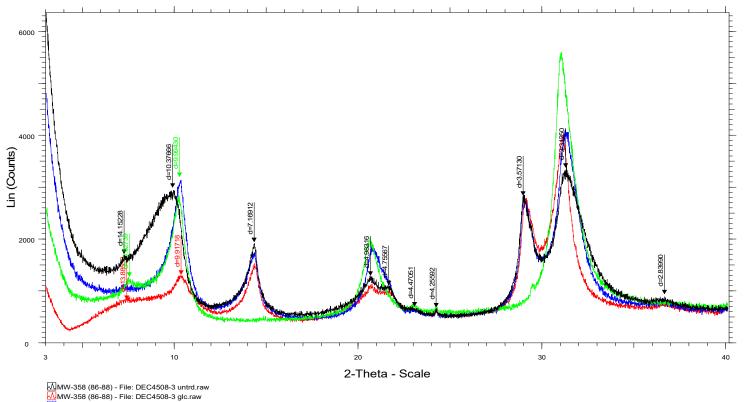




SGS Natural Resources, P.O. Box 4300, 185 Concession Street, Lakefield, Ontario, Canada KOL 2H0



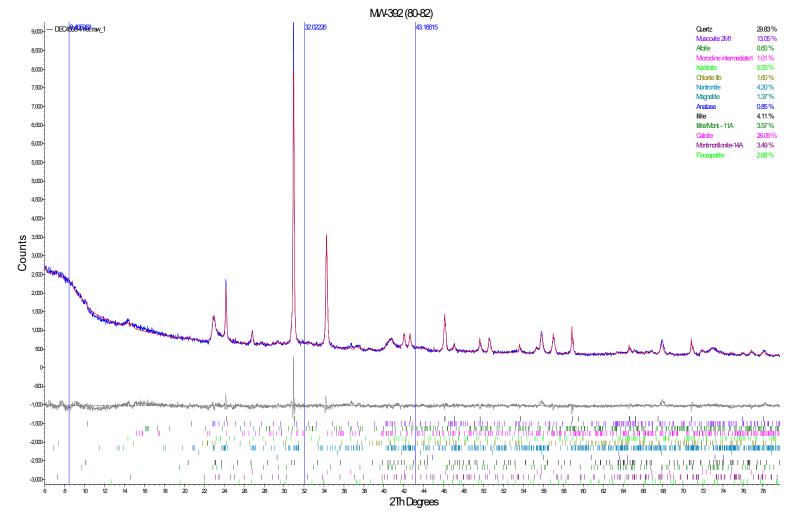
MW-358 (86-88)



MW-358 (86-88) - File: DEC4508-3 400.raw MW-358 (86-88) - File: DEC4508-3 550.raw



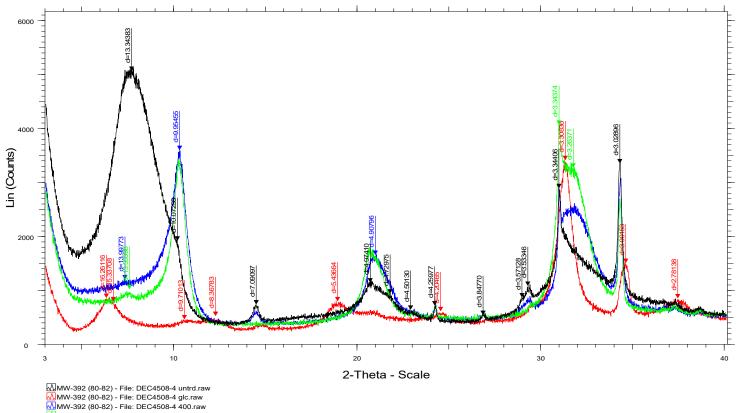
Environmental Services Custom XRD/MI4508-DEC22 24-Apr-23



SGS Natural Resources, P.O. Box 4300, 185 Concession Street, Lakefield, Ontario, Canada KOL 2H0

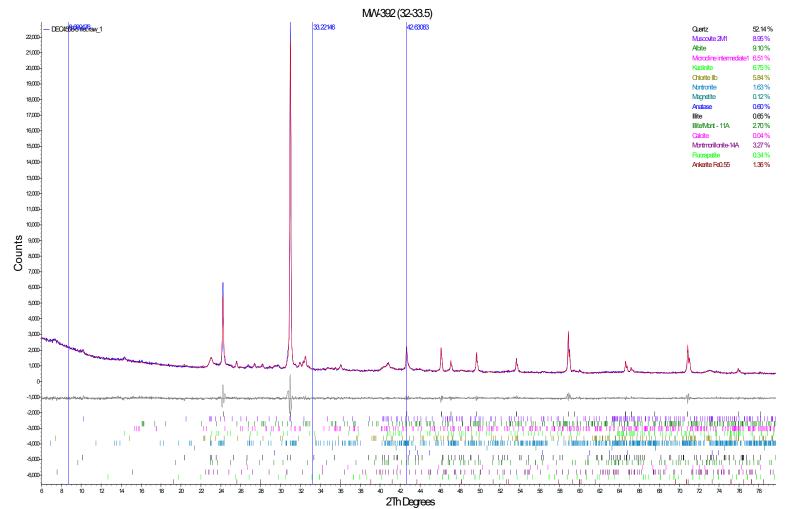


MW-392 (80-82)



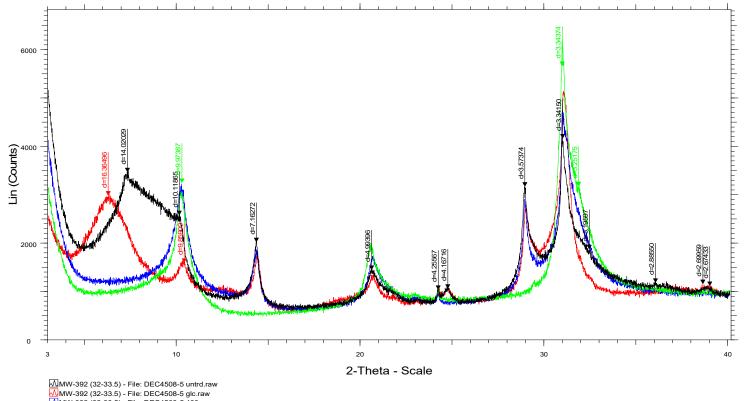
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MW-392 (32-33.5)

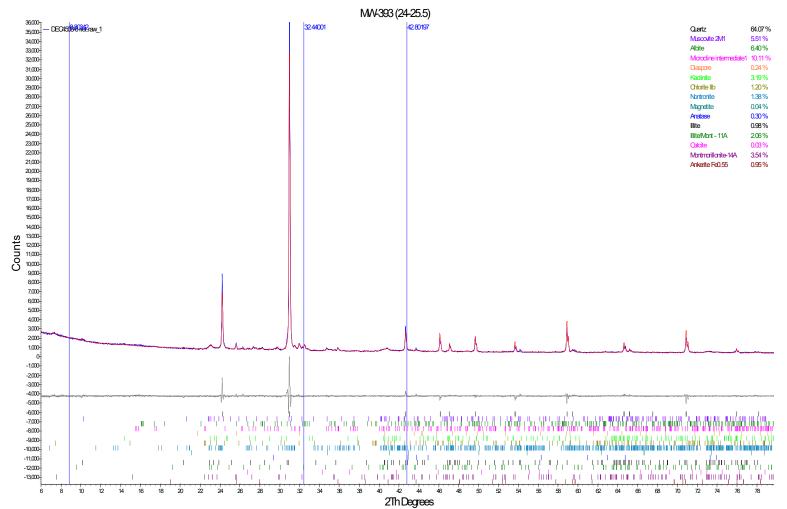


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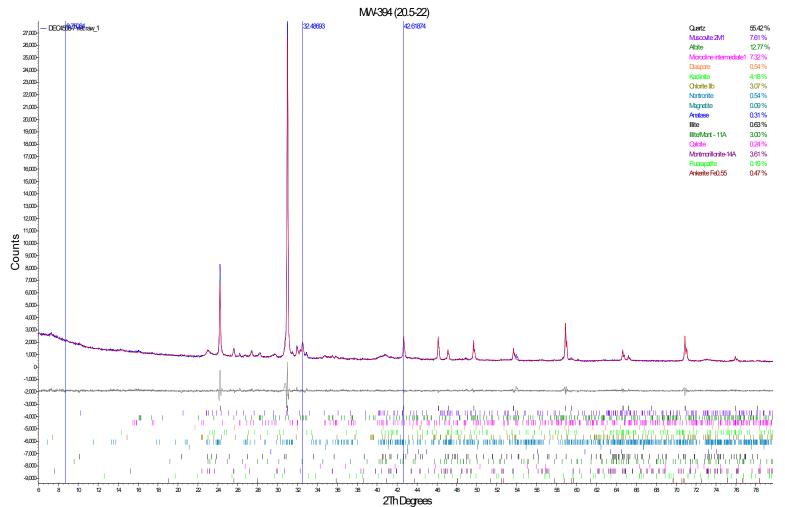
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 MW-392 (32-33.5) - File: DEC4508-5 550.raw

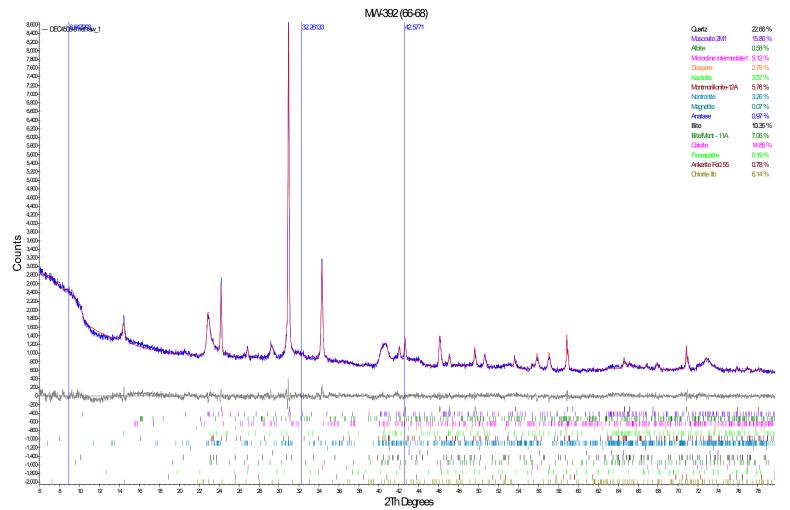






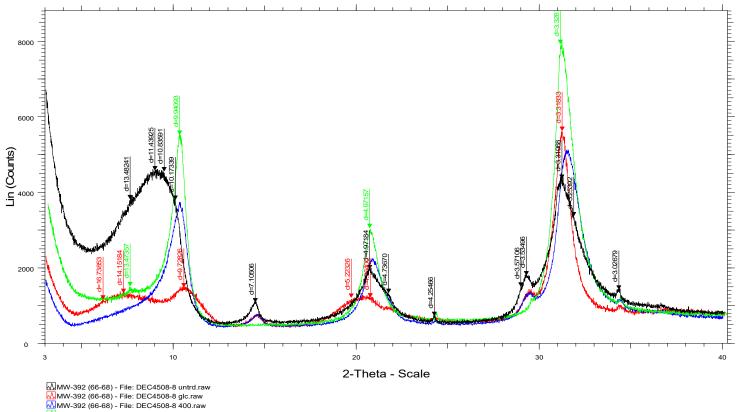








MW-392 (66-68)



MW-392 (66-68) - File: DEC4508-8 550.raw